SAS

# Use of ANN and General Factorial Method to Predict Performance of Maize Dehusker cum Sheller based on Seed Quality Parameters 

Rudragouda Chilur ${ }^{1}$, Naveen Kumar Mahanti ${ }^{1}$, Sushilendra ${ }^{2}$ and V. Bhushana Babu ${ }^{1}$<br>${ }^{1}$ ICAR-Central Institute of Agricultural Engineering, Bhopal<br>${ }^{2}$ University of Agricultural Sciences, Raichur

Received 28 July 2018; Revised 19 July 2019; Accepted 08 August 2019


#### Abstract

SUMMARY India is the third largest producer of maize, where the majority of land holdings are of small (1-2 ha) and medium (2-4 ha) size. Dehusking and shelling are two major operations carried out after harvesting of maize. Farmers need a dehusker cum sheller with medium capacity that suits their requirement for successful adoption in maize growing regions of India. In the present study, the electric motor ( 2.23 kW ) operated Maize Dehusker cum Sheller (MDS) performance was assessed for different combinations of operational parameters, viz. cylinder peripheral speed (PS) (6.2, 6.6, $7.1 \& 7.6 \mathrm{~m} / \mathrm{s})$, concave clearance (CC) $(20,25,30 \& 35 \mathrm{~mm})$ and feed rate (FR) $(400,600 \& 800 \mathrm{~kg} / \mathrm{h})$ and evaluation carried against response variables,viz., Dehusking efficiency (DE), \%; Shelling efficiency (Sh.E), \%; Broken grain losses (BG), \%; seed coat damage (SCD), \%; and germination percentage (GE), \%. The optimization of operational parameters of the machine was done using a numerical optimization technique and performance was evaluated based on response variables using quadratic and artificial neural network (ANN) models. The performance of these models was evaluated based on their $\mathrm{R}^{2}$, SSE, and RMSE. The optimum operating conditions for MDS with a desirability value of 0.85 are $6.77 \mathrm{~m} / \mathrm{s}$ of PS, 27.08 mm of CC and $630.46 \mathrm{~kg} / \mathrm{h}$ of FR. The response variables obtained from these optimum operating parameters were $96.57 \%, 99.53 \%$, $0.751 \%, 99.306 \%$ and $1.792 \%$ for DE, Sh.E, BG, GE, and SCD, respectively. The ANN is a good tool to express the relationship between operating parameters and response variables as compared to the quadratic model.


Keywords: Maize, Seed quality, ANN model, Quadratic model, Optimization.

## 1. INTRODUCTION

In developing countries like India, the agricultural productions system is the main source of livelihood for one-third of the population. The farmers' dependency on food and fodder supplementing with main crops of cultivation rather than selling commercial crop produce for capital generation (Chaudhary et al.,2012; Chilur et al., 2014b). As per the study of Directorate of Maize Research, livestock production is contributing $7 \%$ to National GDP and a source of employment and livelihood for $70 \%$ of the population in rural areas. In addition, climate change presents a major risk to long-term food security as it may decline wheat and maize yield by 5 to $10 \%$ by 2050 (Anonymous, 2016). In the world, India ranks third in maize production $(24.17 \mathrm{mt})$ and fifth in the area ( $9.06 \mathrm{~m}-\mathrm{ha}$ ) during 2013-14. In India, maize is grown in all the seasons
(Anonymous, 2013), where Karnataka is the second largest maize producing $(4.1 \mathrm{mt})$ state contributing to $17 \%$ of total country's production after Andhra Pradesh (Anonymous, 2016b).

Traditionally, dehusking and shelling of maize is carried out manually that involves a lot of drudgery (Mudgal et al., 1998, Singh, 2010, Kumar, 2011, Anonymous, 2012). The output of manual separation is reported to be $30 \mathrm{~kg} / \mathrm{h}$ with shelling efficiency $80-100 \%$, grain damage $0-8.3 \%$ (Mudgal et al. 1998, Anonymous. 2005).The capacity of manually operated shellers ( $27-150 \mathrm{~kg} / \mathrm{h}$ ) is suitable for marginal farmers (Chilur et al., 2014a), where as engine operated ( $1000-1800 \mathrm{~kg} / \mathrm{h}$ ) and tractor operated ( $>2000 \mathrm{~kg} / \mathrm{h}$ ) maize shellers are suitable for large farmers. There are no machines to fulfil the requirement of small and medium farmers with a capacity of $200-1000 \mathrm{~kg} / \mathrm{h}$.

Since, $80.3 \%$ of farmers in the country comes under small and medium group cultivating $36 \%$ of the area (Kumar, 2011). The MDS (Maize dehusker cum sheller) was developed with a capacity of 400-600 $\mathrm{kg} / \mathrm{h}$ by considering the machine performance and seed quality aspects.

Though many researchers have evaluated different machine performance aspects (dehusking efficiency (DE), shelling efficiency (Sh.E), losses (blower, sieve, total), brokens), till now, no research has been carried out on seed quality parameters, viz., seed-coat damage (SCD) and germination percentage (GE) (Sachin, 2008; Tastra, 2009; Tiwari et al., 2010; Chilur et al., 2014c; Vyavahare and Kallurkar, 2015). Therefore, the performance of the developed MDS was optimized including seed quality parameters using artificial neural network (ANN).

ANNs are a general class of non-linear models (Morse et al., 2011; Sharma \& Sawhney, 2015; Sharma et al., 2014a). These are heuristic models, recognized as good tools for dynamic modelling and it is a useful tool for nonparametric regression. ANN model does not require knowledge, assumptions, predefined mathematical relationship, explicit expressions, and inputs-outputs relationships about the nature of undergoing phenomenological mechanisms (Aghbashlo et al., 2015). When the relation between explanatory and response variables is complicated, in that case ANN is a good tool to develop amodel (Omid et al., 2009; Sharma et al., 2013, 2014b). The aim of
the present research is optimization of operational parameters and development of the ANN model; and to compare the same with a quadratic model for also developed in the study, for best prediction of response variables.

## 2. MATERIALS AND METHODS

### 2.1 Study of machine and seed parameters

The engineering properties (viz., physical, aerodynamical and frictional) of most commonly growing maize varieties (viz.,Mahyco (Hero 550), Hema hybrid variety, Ganga Kaveri (GK-3090) and CP818) were used as suggested by Chilur and Sushilendra (2016) and considered in design of MDS (Mohsenin 1970, Jayan and Kumar 2004, El-Fawal et al.,2009, Coskun et al., 2006). The developed MDS was investigated under live conditions in the laboratory and was furthermore, evaluated on-farm with CP 818 maize variety in CAE, Raichur ( $16.205057^{\circ} \mathrm{N}, 77.329972^{\circ}$ E), and Agricultural Research Station, Siraguppa (15.630577 ${ }^{\circ}$ $\mathrm{N}, 76.916559^{\circ} \mathrm{E}$ ), respectively. The working principle of machine and procedure followed for performance evaluation were discussed elsewhere (Chilur et al., 2014c; Chilur and Sushilendra, 2017).

Performance evaluation of developed MDS was carried in accordance with procedure and guidelines prescribed by the Indian standard test codes IS: 7051-1973 and IS: 6284-1985 for maize and cereals, respectively. The machine operating parameters and response variables used in this study are shown in


Fig. 1. The line diagram and pictorial view of developed maize dehusker cum sheller (MDS)

Table 1. The operational and response parameters used in the study

| Independent/Operational parameters |  |  |  | Response variables of seed-quality |
| :---: | :---: | :---: | :---: | :---: |
|  | Levels | Description | Value |  |
| Cylinder peripheral speed (PS), m/s | 4 | $\mathrm{S}_{1}$ | 6.2 | 1. Dehusking efficiency (DE), \% <br> 2. Shelling efficiency (Sh.E), \% <br> 3. Broken grain losses (BG), \% <br> 4. Germination percentage (GE), \% <br> 5. Seed-coat damage (SCD), \% |
|  |  | $\mathrm{S}_{2}$ | 6.6 |  |
|  |  | $\mathrm{S}_{3}$ | 7.1 |  |
|  |  | $\mathrm{S}_{4}$ | 7.6 |  |
| Concave clearance (CC), mm | 4 | $\mathrm{C}_{1}$ | 20 |  |
|  |  | $\mathrm{C}_{2}$ | 25 |  |
|  |  | $\mathrm{C}_{3}$ | 30 |  |
|  |  | $\mathrm{C}_{4}$ | 35 |  |
| Feed rate (FR), $\mathrm{kg} / \mathrm{h}$ | 3 | $\mathrm{F}_{1}$ | 400 |  |
|  |  | $\mathrm{F}_{2}$ | 600 |  |
|  |  | $\mathrm{F}_{3}$ | 800 |  |

Table 2. Different equations of dependent parameters used for performance study

| Dependent variable | Equation | Terms | Reference |
| :--- | :---: | :--- | :---: |
| 1. Dehusking efficiency <br> (DE), \% | $\mathrm{DE}=\left[1-\frac{\mathrm{G}}{\mathrm{H}}\right] \times 100$ | $\mathrm{G}=$ Number of un-dehusked cobs in test run of 25 kg <br> $\mathrm{H}=$ Total number of cobs in test run of 25 kg | Tiwari et al. 2010; |
| 2. Shelling efficiency <br> (Sh.E), \% | $\mathrm{Sh} . \mathrm{E}=\left(100-\mathrm{T}_{\mathrm{u}}\right)$ <br> $\mathrm{T}_{\mathrm{u}}=\frac{\mathrm{D}}{\mathrm{A}} \times 100$ <br> $\mathrm{~A}=\mathrm{B}+\mathrm{C}+\mathrm{D}$ | $\mathrm{T}_{\mathrm{u}}=$ Unthreshed grain, \% <br> $\mathrm{D}=$ Quantity of unthreshed grain obtained from all outlets per unit time <br> $\mathrm{A}=$ Total grain input per unit time <br> $\mathrm{B}=$ Quantity of clean grain from all outlets per unit time <br> $\mathrm{C}=$ Quantity of broken grain from all outlets per unit time | Desta and Mishra 1990; <br> IS: 7051-1973; <br> Beheraet al. (1990); <br> Muhammad (2009) |
| 3. Broken grain losses <br> (BG), \% | $\mathrm{BG}=\frac{\mathrm{C}}{\mathrm{A}} \times 100$ | $\mathrm{A}=$ Total grain input per unit time <br> $\mathrm{C}=$ Quantity of broken grain from all outlets per unit time | Tastra, 2009 |
| 4. Seed-coat damage <br> (SCD), \% | $\mathrm{SD}=\frac{\mathrm{L}}{\mathrm{K}} \times 100$ | $\mathrm{~L}=$ Number of black coloured seeds in test | Copeland and <br> McDonald, 2010 |
| 5. Germination <br> percentage (GE), \% | $\mathrm{GE}=\frac{\mathrm{J}}{\mathrm{K}} \times 100$ | $\mathrm{J}=$ Number of grains were germinated at the end of II count <br> $\mathrm{K}=$ Total number of seeds used in the test | Bansal and Kumar, 2009 |

Table 1. The different equations used to calculate the response variables are illustrated in Table 2.

### 2.2 Data analysis and optimization

Statistical data analysis was done by the asymmetric factorial experiment laid in Completely Randomized Design (CRD) with 3 replications for each combination of PS, CC, and FR factors. The operating parameters of MDS were optimized by numerical optimization technique using Design Expert ${ }^{\circledR}$ Version 7.0.0 (developed by Stat-Ease, Inc., 2021 East Hennepin Ave., Suite 480, Manneapolis-55413) package. Which was based on desirability value constructed on response variables. Myers and Montgomery, 2002 described that the desirability is unitless numerical measure
(Varies 0 to 1 ) of identifying the best combination for peak optimal performance of responses (Dependent variable) from factors (Independent variable). The set of constraints, viz., maximization (for DE, Sh.E, and GE ), minimization (for BG , and SCD ) and in-therange (for PS, CC, and FR) were applied to variables to find desirability value. Similarly, an equal level of importance ("+++") was chosen for all dependents. The optimized operational parameters combination were chosen against the highest value of desirability obtained against a particular treatment combination (Montgomery, 2001). The 3D surface was obtained and inferences were drawn against optimized operating conditions individually for all the response variables studied.

### 2.3 Modelling

### 2.3.1 Non-linear regression (Quadratic function) modelling

The general factorial method was used to determine the optimum operating parameters for the performance evaluation of MDS. The operating parameters selected for the study were listed in Table 1. Regression analysis was carried out three times (triplicate), to estimate the variability of measurements. The relationship between the operating parameters and the response variables was calculated by using the following second-order polynomial equation (quadratic function) (Eq.1)

$$
\begin{equation*}
\mathrm{Y}=\beta_{0}+\sum_{\mathrm{i}=0}^{\mathrm{k}} \beta_{\mathrm{i}} \mathrm{X}_{\mathrm{i}}+\sum_{\mathrm{i}=0}^{\mathrm{k}} \beta_{\mathrm{ii}} \mathrm{X}_{\mathrm{i}}^{2}+\sum_{\mathrm{i}=1}^{\mathrm{k}-1} \sum_{\mathrm{j}=\mathrm{i}+1}^{\mathrm{k}} \beta_{\mathrm{ij}} \mathrm{X}_{\mathrm{i}} \mathrm{X}_{\mathrm{j}} \tag{1}
\end{equation*}
$$

Where, $\mathrm{Y}=$ predicted response; $\beta_{0}=$ constant; $\beta_{\mathrm{i}}=$ linear coefficient; $\beta_{\mathrm{j}}=$ squared coefficient; $\beta_{\mathrm{ij}}=$ cross product coefficient and $\mathrm{k}=$ number of factors.

### 2.3.2 Configuration of ANN

A feed forward back propagation neural network with topology comprising two layers was empirically found to be optimum in this study for the prediction of performance characteristics of maize dehusker cum sheller. The number of neurons in the input layer is equal to the number of independent variables, i.e., PS, CC and FR; the number of output neurons is equal to the number of dependent variables, i.e., DE, Sh.E, BG, SCD and GE. There is no hard and fast rule for determining the required number of hidden neurons in a hidden layer (Huang and Mujumdar, 1993). The number of neurons in the hidden layer was selected based on the trail and error method by varying from 2 to 100 and the optimum number of neurons were finalized based on the statistical parameters (coefficient


Fig. 2. The structure of a multilayer feed forward artificial neural network used.
of determination $\left(\mathrm{R}^{2}\right)$, root mean square error (RMSE), and error sum of squares (SSE). The structure of a multilayer feed forward back propagation artificial neural network (FFANN) used in the present study is shown in Fig. 2.

## Normalization of data

In the process of network learning, it is necessary to preprocess the sample data to make training easy and to reflect better correlations among them (Peng et al., 2007). The whole input data are scaled within the range of 0 to 1 . The normalization is required in order to obtain good results as well as to fasten up significantly the learning (Sola and Sevilla, 1997). The normalization of data is carried out using the minimummaximum technique (Eq.2).

Normalized input data

$$
\begin{equation*}
N_{I}=\frac{N_{i}-N_{i \min }}{N_{i \operatorname{imax}}-N_{i \min }} \tag{2}
\end{equation*}
$$

Where,

$$
\begin{aligned}
& \mathrm{N}_{\mathrm{imin}}=\text { the minimum input data } \\
& \mathrm{N}_{\mathrm{imax}}=\text { the maximum input data } \\
& \mathrm{Ni}=\text { the values before normalization } \\
& \mathrm{N}_{\mathrm{I}}=\text { the values after normalization } \\
& \text { Network learning }
\end{aligned}
$$

A total of 144 experiments were conducted with three replications as given in Table 1 and the experimental data were used for training and testing the selected network. The training was done with $70 \%$ of the experimental data and the remaining $30 \%$ of the data were used for testing the performance of the network, similarly $k$-fold cross validation method was also employed with three folds. JMP Pro10 Software was used for training the neural network and testing its performance. The activation function for the hidden layer and output layer of the network were taken as a hyperbolic function $\left[\tanh =\left(\mathrm{e}^{2 x}-1\right) /\left(\mathrm{e}^{2 x}+1\right)\right.$ ] and linear function, respectively. The training algorithm used for updating the weights of the input layer to the hidden layer and hidden layer to output layer connections was the quasi-Newton method, BFGS (Broyden-Fletcher-Goldfarb-Shanno) algorithm. As the BFGS iterations proceed, the value of the likelihood function of the model on the validation data is monitored. When the cross-validation likelihood is no longer improving, the BFGS algorithm will terminate. This is commonly referred to as the early stopping rule. The network
learning was carried out with a learning rate of 0.2 and the number of tours equal to 100 (both the values were determined empirically). The iteration with best validation statistics is chosen as the final model. The statistical parameters obtained from validation data was used to evaluate the performance of the model. The $\mathrm{R}^{2}$, RMSE (Eq.3), and SSE (Eq.4) were used to evaluate the performance of the model. The penalty squared method $\left(\Sigma \beta^{2}{ }_{\mathrm{i}}\right)$ was used to extenuate the over fitting of the model

$$
\begin{equation*}
\text { RMSE }=\sqrt{\frac{\sum_{i=1}^{n}\left(\hat{y_{1}}-y_{i}\right)^{2}}{n}} \tag{3}
\end{equation*}
$$

Where $y_{i}$ is the observed value for the $i^{\text {th }}$ observation and $\bar{y}_{i}$ is the predicted value.
$\operatorname{SSE}=\sum_{\mathrm{i}=1}^{\mathrm{n}}\left(\mathrm{y}_{\mathrm{i}}-\overline{\mathrm{y}}\right)^{2}$
$y_{i}$ is the value of the $i^{\text {th }}$ observation and $\bar{y}$ is the mean of all the observations

## 3. RESULTS AND DISCUSSIONS

### 3.1 Optimization of operational parameters of MDS

The desirability curve among operating parameters at optimum FR ( $630.46 \mathrm{~kg} / \mathrm{h}$ ) is shown in Fig 3. The maximum desirability value obtained was 0.85 at 6.77 $\mathrm{m} / \mathrm{s}$ of PS, 27.10 mm of CC and $630.46 \mathrm{~kg} / \mathrm{h}$ of FR, it is shown (Flag location) in Fig. 3a.

### 3.2 Quadratic model

The estimated coefficients ( $\beta$ ), standard error (SE) and level of significance obtained after fitting experimental data with the quadratic function of different response variables are listed in Table 3. From Table 3, it is clear that some of the operating parameters are significant and some are non-significant. In case of DE , all the operating parameters are significant except for the square of feed rate $\left(\mathrm{FR}^{2}\right)$. The interaction effect of FR with CC and PS (FR-CC and FR-PS) are nonsignificant in Sh.E. In case of BG, all the operating parameters are significant except the interaction effect of PS with CC and FR (PS-CC and PS-FR) and the square of $\mathrm{FR}\left(\mathrm{FR}^{2}\right)$. In the case of SCD and GE except for the interaction effect of FR with CC and PS (FRCC and FR-PS) and the square of $\mathrm{FR}\left(\mathrm{FR}^{2}\right)$ were nonsignificant. The quadratic model for GE by combining coefficients in Table 3 is in the following form (Eq.5).

$$
\begin{align*}
& \mathrm{GE}=99.073-1.423 \mathrm{~S}+0.622 \mathrm{C}+0.289 \mathrm{~F}+0.177 \mathrm{SC}+ \\
& 0.047 \mathrm{SF}+0.098 \mathrm{CF}-0.999 \mathrm{~S}^{2}-0.303 \mathrm{C}^{2}-0.073 \mathrm{~F}^{2} \tag{5}
\end{align*}
$$

The response variables obtained at optimum operating parameters were $96.57 \%, 99.53 \%, 0.751 \%$, $99.306 \%$ and $1.792 \%$ for DE, Sh.E, BG, GE and SCD, respectively.

### 3.3 Performance measures

### 3.31 Dehusking efficiency (DE)

The effect of PS, CC, FR and their interaction on DE is shown in Fig. 5. The DE decreased with increase in CC for all PS at constant FR because of increase in CC makes less dense cobs inside leads to less abrasion and further cob moves towards the outlet in a shorter time it leads to decrease in dehusking action, it is shown in Fig. 5a. Similar findings have been reported by Singh (2010). The effect of feed rate on DE w.r.t. CC and PS is shown in Fig. 5b. The DE increased up to a certain level of FR at constant CC and PS and decreased thereafter. The DE increased with an increase in peripheral speed up to $7 \mathrm{~m} / \mathrm{s}$ at constant FR and CC thereafter there is no effect has been observed with an increase in PS, it is shown in Fig. 5c. The interaction effect of PS and FR is highly significant ( 0.0008 ) followed by PS and CC (0.0076) and CC and FR (0.0193) (Table 3).

### 3.3.2 Shelling efficiency (Sh.E)

The effect of different operating parameters and their interaction on Sh.E of MDS is shown in Fig.6. The Sh.E increased with increasing CC from 20 mm to 25 mm and thereafter it reduces with increasing CC at a given PS and FR of $630.46 \mathrm{~kg} / \mathrm{h}$ (Fig.6a). The Sh.E increases up to a certain level with an increase in FR and thereafter it starts declining at constant CC and PS of $6.77 \mathrm{~m} / \mathrm{s}$ (Fig.6b). This trend is due to less energy spent per cob in terms of less number of impacts were taken place on cobs for the same length of the cylinder and due to cushioning effect at higher FR caused to decrease the Sh.E. The similar results were reported by Vas and Harrison (1969) and Singh (2010). The increase in PS leads to increase in Sh.E up to $7 \mathrm{~m} / \mathrm{s}$ at any FR and constant CC ( 27.08 mm ) due to the increased detachment with higher impacts and friction created between the cylinder and concave, it is shown in Fig.6c. The further increase in PS leads to decrease in Sh.E due to less retention time of cobs in concave and it might have an increasing conveyance of plant mass by angled ( $45^{\circ}$ ) lugs arrangement (Chilur and Sushilendra, 2017). The interaction effect of PS and CC is significant (0.0002) and has a negative impact on Sh.E, while the remaining interactions (PS-FR and CC-FR) are non-significant (Table 3).


Fig. 3. Desirability contours (a) and 3D surface (b) based on different seed quality parameters against concave clearance and cylinder peripheral speed for developed MDS at the centre value of feed rate, i.e., $630.46 \mathrm{~kg} / \mathrm{h}$

Table 3. The estimated coefficient ( $\beta$ ), standard error (SE) and their significance of individual and interaction effect ( $p$-value) on different response variables were fitted with aquadratic function

| Factor | DE, \% |  | Sh.E, \% |  | BG, \% |  | GE, \% |  | SCD, \% |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\beta$ (SE) | p | $\beta$ (SE) | p | $\beta$ (SE) | p | $\beta$ (SE) | p | $\beta$ (SE) | p |
| Int. | 97.262(0.294) | $<0.0001$ | 99.932(0.182) | $<0.0001$ | 0.838(0.038) | $<0.0001$ | 99.073(0.121) | $<0.0001$ | 2.049(0.123) | $<0.0001$ |
| PS | $3.547(0.156)$ | $<0.0001$ | $1.638(0.097)$ | $<0.0001$ | 0.501(0.02) | $<0.0001$ | -1.423(0.064) | $<0.0001$ | $1.565(0.066)$ | $<0.0001$ |
| CC | -3.688(0.158) | $<0.0001$ | -1.53(0.098) | $<0.0001$ | -0.318(0.021) | $<0.0001$ | $0.622(0.065)$ | $<0.0001$ | -0.621(0.066) | $<0.0001$ |
| FR | -1.138(0.144) | $<0.0001$ | -0.394(0.089) | $<0.0001$ | -0.161(0.019) | $<0.0001$ | $0.289(0.059)$ | $<0.0001$ | -0.292(0.061) | $<0.0001$ |
| PS-CC | $0.567(0.209)$ | 0.0076 | -0.503(0.13) | 0.0002 | 0.009(0.027) | 0.7522 | $0.177(0.086)$ | 0.0411 | -0.178(0.088) | 0.0445 |
| PS-FR | 0.653(0.191) | 0.0008 | $0.228(0.119)$ | 0.0558 | -0.021(0.025) | 0.4090 | 0.047(0.079) | 0.5576 | -0.045(0.08) | 0.5798 |
| CC-FR | -0.456(0.193) | 0.0193 | -0.218(0.12) | 0.0702 | $0.068(0.025)$ | 0.0072 | $0.098(0.079)$ | 0.2195 | -0.099(0.081) | 0.2222 |
| $\mathrm{PS}^{2}$ | -1.904(0.27) | $<0.0001$ | -2.638(0.167) | $<0.0001$ | $0.327(0.035)$ | $<0.0001$ | -0.999(0.111) | $<0.0001$ | 1.071(0.113) | $<0.0001$ |
| $\mathrm{CC}^{2}$ | -1.794(0.264) | $<0.0001$ | -1.444(0.164) | $<0.0001$ | $0.235(0.034)$ | $<0.0001$ | -0.303(0.109) | 0.0060 | 0.299(0.111) | 0.0077 |
| $\mathrm{FR}^{2}$ | -0.114(0.249) | 0.6488 | -0.983(0.154) | $<0.0001$ | $0.031(0.032)$ | 0.3322 | -0.073(0.102) | 0.4780 | 0.075(0.105) | 0.4727 |

### 3.3.3 Broken grain losses (BG)

The BG majorly depends on the operational parameters. The effect of operational parameters CC, PS, FR and their interaction on BG is shown in Fig.7. The BG decreased with increasing CC for all PS and constant FR of $630.46 \mathrm{~kg} / \mathrm{h}$ (Fig.7a), since the impact by cylinder lugs on less number of grains in each revolution of the cylinder may be attributed as the reason for decreased BG (Akubuo, 2002). Similarly, the increase in FR leads to decrease in a decrease in BG for all CC and constant PS of $6.77 \mathrm{~m} / \mathrm{s}$ (Fig.7b). The BG increases with increase in PS for all FR and constant CC of 27.08 mm (Fig.7c). The interaction effect of PS with CC and FR are found to be non-significant, but the interaction effect of CC and FR was significant ( 0.0072 ) on BG (Table 3).

### 3.3.4 Germination percentage (GE)

The maize has higher GE as compared to other cereals (Anon. 2016a), the minimum GE obtained in the present study was $94 \%$ and maximum up to $99 \%$. The grain GE majorly depends upon the operating levels of MDS, so it is necessary to study the effect of operating parameters and their interaction effect on GE. The effect of operational parameters (CC, PS, and FR) and their interaction on GE is shown in Fig. 8. The GE increased with increasing CC for all PS and constant FR ( $630.46 \mathrm{~kg} / \mathrm{h}$ ), it is shown in Fig.8a. Similarly, FR also has a positive effect for all CC and constant PS of $6.77 \mathrm{~m} / \mathrm{s}$ (Fig. 8b), but PS has a negative effect on GE for all FR and constant CC ( 27.08 mm ) (Fig. 8c). The result shows that the percentage of non-germinated seeds was higher as compared to the BG, which means
some of the unbroken seeds also not get germinated may be due to mechanical damage of embryo, seedcoat, etc. to obtain the greater GE of the MDS, it is recommended that the PS should be low, high, CC and optimum FR. The interaction effect of FR with CC and PS was non-significant and the interaction effect of PS with CC was significant (0.0411) (Table 3).

### 3.3.5 Seed-coat damage percentage (SCD)

The germination of the seed depends upon the SCD also, so it is necessary to know the effect of operational parameters on SCD. The effect of operational parameters and their interaction on SCD is shown in Fig.9. From this, it is clear that SCD decreases with increase in CC for all PS and constant FR $630.46 \mathrm{~kg} / \mathrm{h}$ (Fig.9a). Similarly, an increase in FR also has positive effect on SCD for all CC and constant PS ( $6.77 \mathrm{~m} / \mathrm{s}$ ) (Fig.9b). But the increase in PS has a negative impact on SCD for all FR and constant CC of 27.08 mm (Fig.9c).The interaction effect of FR with CC and PS was non-significant, while the interaction effect of PS and CC are found to be significant (Table 3). The maximum SCD ( $5.90 \%$ ) was observed at higher PS and lower CC and FR, while the minimum SCD (1\%)
was observed at lower PS and higher FR and CC. The mechanical damage of maize was observed in the range of 6.38 to $16 \%$ by Chowdhury and Buchele (1976) and Singh et al. (2011) for conventional combines whereas, in this study it was less ( 1 to $6 \%$ ) due to lower operating speed compare to combine threshing drum speed ( $>20$ $\mathrm{m} / \mathrm{s}$ ) and angled lugs threshing drum design. The lesser damage in developed MDS may be due to the use of chamfered lugs on the cylinder and the helical arrangement which not sustenance to augment of SCD. From the reviewed data of Handbook, the PS was recommended as $9 \mathrm{~m} / \mathrm{s}$ for dehusking and shelling of maize cobs (Anon., 2004). Since the present problem to produce maize grains for seeding purpose, the lower speed, i.e., below $7.1 \mathrm{~m} / \mathrm{s}$ was found in agreement with concern to seed-quality aspects.

### 3.4 ANN modelling

ANN model for different machine performance parameters was developed using $70 \%$ of data and the developed model was validated using $30 \%$ of data. The performance of the model was tested at a different number of hidden neurons (2-100) and the optimum number of neurons for all the response variables was


Fig. 5. The effect of PS, CC and FR factors on DE at optimized FR (a) at optimized PS (b) and at optimized CC (c)


Fig. 6. The effect of PS, CC and FR factors on Sh.E at optimized FR (a) at optimized PS (b) and at optimized CC (c)


Fig. 7. The effect of PS, CC and FR factors on BG at optimized FR (a) at optimized PS (b) and at optimized CC (c)


Fig. 8. The effect of PS, CC and FR factors on GE at optimized FR (a) at optimized PS (b) and at optimized CC (c)


Fig. 9. The effect of PS, CC and FR factors on SCD at optimized FR (a) at optimized PS (b) and at optimized CC (c)
optimised based on the minimum error and maximum $R^{2}$ value. The statistical results for different response variables at a different number of hidden neurons for hold back and k -fold cross validation methods were listed in the Appendix. The optimum number of neurons for DE, Sh.E, BG, SCD, and GE in hold back and k -fold validation methods are tabulated in Table 4. The optimum number of neurons in both the validation methods were too high. More than $94 \%$ accuracy of the model is obtaining within the 10 neurons but to increase the accuracy by $2 \%$ it is necessary to select
the optimum number of neurons which may lead to over fitting and increase in complexity of the model. Therefore, it is recommended to select the number of hidden neurons as low as possible. The k-fold cross validation method is advisable for a small data set and hold back method is suitable for a large data set.

### 3.5 Comparison of quadratic and ANN modelling

The comparison between QF and ANN modelling was done using statistical parameters, viz., RMSE, SSE, and $R^{2}$. The statistical parameters obtained from QF

Table 4. Statistical results obtained from fitting experimental data with quadratic and ANN model

| Response variables | Quadratic function |  |  | ANN-Model (Holdback) |  |  |  | ANN-Model (k-Fold) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{R}^{2}$ | RMSE | SSE | Optimum neurons | $\mathbf{R}^{2}$ | RMSE | SSE | Optimum neurons | $\mathbf{R}^{2}$ | RMSE | SSE |
| DE | 0.9036 | 5.0824 | 2479.75 | 88 | 0.95 | 1.002 | 44.17 | 65 | 0.984 | 0.586 | 17.857 |
| Sh.E | 0.8742 | 2.7102 | 705.14 | 71 | 0.967 | 0.519 | 11.845 | 83 | 0.961 | 0.476 | 10.863 |
| BG | 0.8933 | 0.6124 | 36 | 60 | 0.963 | 0.128 | 0.720 | 46 | 0.987 | 0.063 | 0.188 |
| SCD | 0.8563 | 1.6969 | 276.45 | 12 | 0.959 | 0.341 | 5.119 | 82 | 0.968 | 0.265 | 3.378 |
| GE | 0.8421 | 1.5726 | 237.43 | 26 | 0.957 | 0.333 | 4.875 | 82 | 0.963 | 0.265 | 3.381 |



Fig. 4. Comparison between actual and predicted values obtained from ANN and quadratic models for the (a) DE, (b) Sh.E, (c) BG, (d) SCDand (e) GE
and ANN modelling of different response variables (at an optimum number of hidden neurons) have been listed in Table 4. From this table, it is clear that the ANN model explained a good relationship between operational parameters and response variables. The plot of predicted data obtained from QF and ANN against experimental data for all response variables is shown in Fig 4. The QF model shows greater deviation than the ANN model. The ANN model shows a greater generalization capacity than the QF model. The higher predictive accuracy of the ANN model was due to the universal ability to approximate the non-linearity of the system, whereas the QF is restricted to a second-order polynomial (Youssefi et al., 2009). Another advantage with ANN over the QF is the ability to calculate multiresponses in a single process. To obtain a multi-response optimization, the QF model must be run several times (equal to the number of the parameters to be predicted) (Youssefi et al., 2009).

## 4. CONCLUSIONS

In this study, the optimization of operational parameters and performance evaluation of maize dehusker cum sheller (MDS) based on seed quality parameters using quadratic and ANN model was conducted. The optimum operating parameters obtained from numerical optimization technique for peripheral speed (PS), concave clearance (CC), and feed rate (FR) were $6.77 \mathrm{~m} / \mathrm{s}, 27.08 \mathrm{~mm}$, and 630.46 $\mathrm{kg} / \mathrm{h}$, respectively. The response variables obtained at optimum operating parameters were $96.57 \%$, $99.53 \%, 0.751 \%, 99.306 \%$ and $1.792 \%$ for dehusking efficiency (DE), shelling efficiency (Sh.E), broken grain losses (BG), germination percentage (GE) and seed coat damage ( SCD ), respectively. The $\mathrm{R}^{2}$ value of the developed quadratic model for all the response variables (DE, SE, BG, GE, and SCD) varies between 0.8421-0.9036, the RMSE values varies between 0.6124-5.0824 and SSE values varies from 36-2479.75. More than $94 \%$ accuracy of the ANN model was achieved within the 10 neurons. The $\mathrm{R}^{2}$, RMSE and SSE values of the developed ANN models for all the response variables were $>0.9,<1.5$ and $<90$, respectively even at below 10 number of hidden neurons. The maximum $\mathrm{R}^{2}$ and minimum error (SSE and RMSE) were observed in case of ANN model over the quadratic model. Hence, the ANN models described the best relationship between operating parameters and response variables. Therefore, ANN is a good tool to assess the performance parameters of MDS.

## ACKNOWLEDGMENT

The author presents the sincere thanks to Head, Dept. of FMPE and Dean, College of Agricultural Engineering, Raichur, Karnataka (India) for providing necessary arrangements, instrumentation and workforce to conduct the study. We sincerely thank and acknowledge the anonymous referee for critically reviewing and giving constructive suggestions for improvement of the manuscript.

## REFERENCES

Aghbashlo, M., Hosseinpour, S. and Mujumdar, A.S. (2015).Application of Artificial Neural Networks (ANNs) in Drying Technology-A Comprehensive Review, Drying Technology, 33(12), 1397-1462.
Akubuo, C.O. (2002). Performance evaluation of a local maize sheller. Biosystems Engineering, 83(1), 77-83.
Anonymous. (2004). Data Book for Agricultural Machinery DesignChapter 9 \& 10. Central Institute of Agricultural Engineering (CIAE), Bhopal-462038, India, 339-396.

Anonymous. (2005). Empowerment of farm women in agriculture. Final Report of MM NATP-20. College of Home Science, MPUAT. Udaipur, 63.
Anonymous. (2012). Maize dehusker cum sheller reduces drudgery in farm women. Success Stories, Directorate of Research on Women in Agric. (ICAR), Bhuvaneswar-75003, Orissa, India.

Anonymous. (2013). State-wise area, production and yield of maize (Kharif+Rabi) in Northern India, (2000-2001 to 2009-2010 and 2011-2012). Indiastat.com, Directorate of Economics \& Statistics, Govt. of India.
Anonymous. (2016). ICAR Vision 2050. Published by Indian Council of Agricultural Research, KrishiBhavan, New Delhi 110 001, India (http://www.icar.org.in/files/Vision-2050-ICAR.pdf)

Anonymous. (2016a). Maize dehusker cum sheller (http://www. amaragri.com/maize_ dehusker\&sheller. html- Accessed on 1 September, 2016)
Anonymous. (2016b). Selected State/Season-wise Area, Production and Productivity of Maize in India (2014-2015). Ministry of Agriculture and Farmers Welfare, Govt. of India.(ON1151). http:// www.indiastat.com/table/agriculture/2/maize/17199/7269/data. aspx.
Bansal, K.N. and Kumar, L.S. (2009). Design and development of an axial flow thresher for seed crops. Journal of Agricultural Engineering, 46(1), 1-8.
Behera, B.K., Dash, S.K. and Das, D.K. (1990). Development and testing of a power operated wheat thresher. Agricultural Mechanization in Asia, Africa, and Latin America,21(4), 15-21.

Chaudhary, D.P., Kumar, A., Sapna, S.M., Srivastava, P. and Kumar, R.S. (2012). Maize As Fodder? An alternative approach. Directorate of Maize Research, Pusa Campus, New Delhi-110 012, Technical Bulletin 2012/04, 32.

Chilur, R. and Sushilendra. (2017). Performance assessment and optimization of maize dehusker cum sheller - A technology for Northern Transition Zone of Karnataka. Ind. J. Agril. Sci., 87(11), 1535-1542.

Chilur, R., Yaranal, R., Yaligar, R., Vasantgouda, B.R., Nagaraj, D.M. and Shashirekha. (2014a). Pedal operated tubular maize sheller-A novel technology for marginal and small farmers. Environment \& Ecology, 32(1A), 239-242.
Chilur, R., Vasantgouda, R., Shashirekha., Yaligar, R., Nagaraj, D.M., Kanannavar, P.S. and Vijayakumar, P. (2014b). The economic investigation of maize cultivation- a state of farmers in Haveri district, Karnataka. Environment \& Ecology, 32(4), 1338-1341.

Chilur, R., Sushilendra., Palled, V., Veeranouda, M., Yaranal, R.S. and Sharangouda, H.(2014c). Effect of operational parameters on dehusking-cum-shelling efficiency and broken grain percentage of maize dehusker-cum-sheller. International Journal of Scientific Research, 3(80), 10-14.
Chowdhury, M.H. and Buchele, W.F. (1976). Development of a numerical damage index for critical evaluation of mechanical damage of corn. Transactions of the ASAE, 19(3), 428-432.
Copeland, O.L. and McDonald, B.M. (2010). Principles of seed science and technology. pp 72-123. $4^{\text {th }}$ edition. Published by Springer (India) Private Limited, New Delhi-110002.

Coskun, B.M., Ibrahim, Y. and Ozarslan, C. (2006). Physical properties of sweet corn seed (Zea mays saccharata Sturt.). Journal of Food Engineering, 74, 523-528.
El-Fawal, Y.A, Tawfik, M.A. and El-Shal, A.M. (2009). Study on physical and engineering properties for grains of some field crops. Misr Journal of Agricultural Engineering, 26(4), 1933-1951.
Ghaly, A.E. (1985). A stationary threshing machine design construction and performance evaluation. Agricultural Mechanization in Asia, Africa, and Latin America, 16(3), 193-195.
Huang, B. and Mujumdar, A.S. (1993). Use of neural network to predict industrial dryer performance. Drying technology, 11(3), 525-541.

Indian Standard. (1973). Specification for maize sheller. IS: 7051-1973, Indian Standard Institution, Manak Bhavan, 9 Bahadur Shah Zafar Marg, New Delhi 110001, 1-7.
Indian Standard. (1985). Test code for power thresher for cereals (Second revision). IS: 6284-1985, Indian Standard Institution, Manak Bhavan, 9 Bahadur Shah Zafar Marg, New Delhi-110001, 1-28.

ISTA. (2013). International Rules for Seed Testing. Seed Science and Technology, 4, 51-177.
Jayan, P.R. and Kumar, V.J.F. (2004). Planter design in relation to the physical properties of seeds. Journal of Tropical Agriculture, 42(1-2), 69-71.
Kumar, N.D.B. (2011). Modification and evaluation of power operated maize (Zeamays L.) sheller. M. Tech. (Ag. Engg.) Thesis, University of Agricultural Sciences, Bengaluru, Karnataka.
Mohsenin, N.N. (1970). Physical properties of plant and animal materials ( $2^{\text {nd }}$ Edn.). Gordon and Breach Science Publications, New York. 56-91
Montgomery, D.C. (2001). Design and Analysis of Experiments. New York "Wiley". 416-419
Morse, G., Jones, R., Thibault, F.J. and Tezel, H. (2011). Neural network modelling of adsorption isotherms. Adsorption, 17, 303-309.
Mudgal, V.D., Jain, N.K., Bordia, J.S. and Seth, P. (1998). Research igest (1992-97) Udaipur Centre. AICRP on PHT, CTAE, Udaipur, 17-18.

Muhammad, D.A. (2009). Design and construction of a maize sheller. Nigerian Defence Academy Kaduna. 7622.
Myers, R.H. and Montgomery, D.C. (2002). Response Surface Methodology: Product and process optimization using designed experiments. $2^{\text {nd }}$ Edition, John Wiley \& Sons, New York.

Omid, M., Baharlooei, A. and Ahmadi, H. (2009). Modeling drying kinetics of pistachio nuts with multilayer feed-forward neural network. Drying Technology, 27, 1069-1077.
Peng, G., Chen, X., Wu, W. and Jiang, X. (2007). Modeling of water sorption isotherm for corn starch. Journal of Food Engineering, 80, 562-567.
Sachin, P. (2008). Design, development and evaluation of a power operated maize sheller (Spiked Disk Type). International Journal of Agricultural Sciences, 4, 215-219.

Sharma, A. K., Jain, D.K., Chakravarty, A.K., Malhotra, R. and Ruhil, A.P. (2013). Predicting economic traits in Murrah buffaloes with connectionist models. J. Ind. Soc. Agril. Statist., 67, 1-11.
Sharma, A.K., Lal, M. and Sawhney, I.K. (2014a). Computational aspects of soft computing models to predict sorption isotherms in Nutrimix (weaning food). Mathematics in Engineering, Science and Aerospace, 5, 105-119.

Sharma, A.K., Sawhney, I.K. and Lal, M. (2014b). Intelligent modelling and analysis of moisture sorption isotherms in milk and pearl millet based weaning food 'fortified Nutirmix'. Drying Technology: An International Journal, 32, 728-741.

Sharma, A.K. and Sawhney, I.K. (2015). Modelling moisture sorption characteristics in dried acid casein using connectionist paradigm vis-à-vis classical methods. Journal of Food Science and Technology, 52, 151-160.
Singh, S.P., Singh, P. and Singh, S. (2011). Status of maize threshing in India. Agril. Mechanization in Asia, Africa and Latin America, 42(3), 21-28.

Singh, S.P. (2010). Ergonomical interventions in developing hand operated maize dehusker-sheller for farm women. Ph.D. (Ag. Engg.) Thesis, MaharanaPratap University of Agriculture and Technology, Udaipur, Rajasthan.
Sola, J. and Sevilla, J. (1997). Importance of input data normalization for the application of neural networks to complex industrial problems. IEEE Transactions on Nuclear Science, 44(3).
Tastra, I. K. (2009). Designing and testing of improved maize sheller. Agril. Mechanization in Asia, Africa and Latin America, 40(1), 12-17.
Tiwari, P.S., Pandey, M.M., Gite, L.P. and Shrivastava, A.K. (2010). Effect of operating speed and cob size on performance of a rotary maize sheller. Journal of Agricultural Engineering, 47(2), 1-8.

Vas, F.M. and Harrison, H.D. (1969). The effect of selected mechanical threshing parameters on kernel damage and threshability of Wheat. Canadian Agricultural Engineering, 11(2), 83-87.
Vyavahare, R.T. and Kallurkar, S.P. (2015). Ergonomic evaluation of maize sheller cum dehusker. International Journal of Current Engineering and Technology, 5(3), 1881-1886.
Youssefi, S., Emam-Djomeh, Z. and Mousavi, S.M. (2009). Comparison of artificial neural network (ann) and response surface methodology (rsm) in the prediction of quality parameters of spray-dried pomegranate juice. Drying Technology, 27, 910-917.

## APPENDIX

Table: Statistical results obtained from ANN modelling for different response variables at a different number of hidden neurons for hold back cross validation method

| No. of neurons | Shelling efficiency, \% |  |  | Dehusking efficiency, \% |  |  | Germination percentage, \% |  |  | Seed coat damage, \% |  |  | Broken grain losses, \% |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{R}^{2}$ | RMSE | SSE | $\mathbf{R}^{2}$ | RMSE | SSE | $\mathbf{R}^{2}$ | RMSE | SSE | $\mathbf{R}^{2}$ | RMSE | SSE | $\mathbf{R}^{2}$ | RMSE | SSE |
| 2 | 0.802 | 1.445 | 91.891 | 0.942 | 1.105 | 53.729 | 0.926 | 0.441 | 8.558 | 0.933 | 0.442 | 8.593 | 0.929 | 0.177 | 1.379 |
| 3 | 0.848 | 1.275 | 71.472 | 0.946 | 1.088 | 52.045 | 0.917 | 0.470 | 9.736 | 0.929 | 0.468 | 9.645 | 0.929 | 0.167 | 1.220 |
| 4 | 0.853 | 1.252 | 68.985 | 0.939 | 1.150 | 58.146 | 0.932 | 0.429 | 8.101 | 0.941 | 0.433 | 8.239 | 0.922 | 0.194 | 1.660 |
| 5 | 0.869 | 1.210 | 64.464 | 0.937 | 1.164 | 59.639 | 0.939 | 0.412 | 7.462 | 0.947 | 0.427 | 8.036 | 0.928 | 0.195 | 1.679 |
| 6 | 0.853 | 1.205 | 63.905 | 0.944 | 1.161 | 59.280 | 0.945 | 0.411 | 7.445 | 0.948 | 0.429 | 8.084 | 0.912 | 0.208 | 1.895 |
| 7 | 0.889 | 1.087 | 52.006 | 0.936 | 1.196 | 62.982 | 0.946 | 0.380 | 6.363 | 0.955 | 0.378 | 6.274 | 0.935 | 0.174 | 1.333 |
| 8 | 0.867 | 1.098 | 53.064 | 0.944 | 1.073 | 50.694 | 0.943 | 0.382 | 6.435 | 0.956 | 0.372 | 6.088 | 0.929 | 0.195 | 1.671 |
| 9 | 0.925 | 0.908 | 36.292 | 0.936 | 1.172 | 60.473 | 0.928 | 0.421 | 7.799 | 0.937 | 0.426 | 7.992 | 0.927 | 0.207 | 1.881 |
| 10 | 0.881 | 1.146 | 57.755 | 0.941 | 1.126 | 55.781 | 0.948 | 0.374 | 6.142 | 0.944 | 0.410 | 7.405 | 0.920 | 0.205 | 1.845 |
| 11 | 0.921 | 0.975 | 41.816 | 0.947 | 1.084 | 51.688 | 0.953 | 0.362 | 5.776 | 0.958 | 0.366 | 5.882 | 0.914 | 0.196 | 1.683 |
| 12 | 0.891 | 0.998 | 43.844 | 0.944 | 1.143 | 57.528 | 0.954 | 0.334 | 4.915 | 0.959 | 0.341 | 5.119 | 0.879 | 0.260 | 2.964 |
| 13 | 0.914 | 1.017 | 45.467 | 0.947 | 1.084 | 51.736 | 0.948 | 0.365 | 5.861 | 0.959 | 0.357 | 5.594 | 0.917 | 0.194 | 1.651 |
| 14 | 0.864 | 1.120 | 55.178 | 0.947 | 1.122 | 55.347 | 0.949 | 0.354 | 5.520 | 0.957 | 0.360 | 5.706 | 0.941 | 0.175 | 1.352 |
| 15 | 0.874 | 1.092 | 52.425 | 0.945 | 1.143 | 57.527 | 0.948 | 0.367 | 5.917 | 0.943 | 0.400 | 7.054 | 0.936 | 0.181 | 1.445 |
| 16 | 0.893 | 1.043 | 47.881 | 0.949 | 1.128 | 56.005 | 0.941 | 0.391 | 6.741 | 0.942 | 0.416 | 7.611 | 0.930 | 0.187 | 1.541 |
| 17 | 0.907 | 1.041 | 47.664 | 0.938 | 1.200 | 63.372 | 0.959 | 0.343 | 5.187 | 0.949 | 0.385 | 6.522 | 0.904 | 0.201 | 1.780 |
| 18 | 0.903 | 0.985 | 42.731 | 0.950 | 1.050 | 48.500 | 0.917 | 0.463 | 9.450 | 0.954 | 0.403 | 7.161 | 0.935 | 0.210 | 1.937 |
| 19 | 0.904 | 0.987 | 42.868 | 0.939 | 1.183 | 61.620 | 0.947 | 0.383 | 6.438 | 0.932 | 0.456 | 9.151 | 0.906 | 0.217 | 2.069 |
| 20 | 0.900 | 1.033 | 46.91 | 0.922 | 1.280 | 72.128 | 0.960 | 0.349 | 5.352 | 0.966 | 0.348 | 5.315 | 0.934 | 0.180 | 1.433 |
| 21 | 0.917 | 0.837 | 30.795 | 0.940 | 1.105 | 53.679 | 0.942 | 0.382 | 6.424 | 0.939 | 0.411 | 7.418 | 0.902 | 0.229 | 2.313 |
| 22 | 0.952 | 0.690 | 20.929 | 0.951 | 1.071 | 50.471 | 0.917 | 0.474 | 9.877 | 0.936 | 0.428 | 8.067 | 0.940 | 0.158 | 1.100 |
| 23 | 0.927 | 0.752 | 24.867 | 0.952 | 1.056 | 49.028 | 0.934 | 0.418 | 7.706 | 0.951 | 0.391 | 6.711 | 0.941 | 0.200 | 1.756 |
| 24 | 0.942 | 0.713 | 22.367 | 0.921 | 1.317 | 76.329 | 0.912 | 0.463 | 9.427 | 0.938 | 0.409 | 7.354 | 0.938 | 0.178 | 1.388 |
| 25 | 0.944 | 0.751 | 24.794 | 0.914 | 1.348 | 79.948 | 0.892 | 0.513 | 11.573 | 0.943 | 0.426 | 7.990 | 0.930 | 0.178 | 1.399 |
| 26 | 0.929 | 0.752 | 24.851 | 0.929 | 1.302 | 74.586 | 0.957 | 0.333 | 4.875 | 0.921 | 0.456 | 9.148 | 0.923 | 0.187 | 1.540 |
| 27 | 0.911 | 0.866 | 33.015 | 0.914 | 1.337 | 78.611 | 0.947 | 0.379 | 6.319 | 0.956 | 0.361 | 5.739 | 0.900 | 0.213 | 1.991 |
| 28 | 0.947 | 0.692 | 21.054 | 0.914 | 1.338 | 78.787 | 0.920 | 0.487 | 10.440 | 0.916 | 0.547 | 13.163 | 0.955 | 0.154 | 1.040 |
| 29 | 0.904 | 0.837 | 30.814 | 0.928 | 1.315 | 76.063 | 0.940 | 0.390 | 6.688 | 0.923 | 0.438 | 8.429 | 0.937 | 0.175 | 1.349 |
| 30 | 0.938 | 0.754 | 25.010 | 0.936 | 1.202 | 63.559 | 0.927 | 0.450 | 8.918 | 0.957 | 0.385 | 6.535 | 0.917 | 0.203 | 1.813 |
| 31 | 0.938 | 0.729 | 23.414 | 0.902 | 1.401 | 86.372 | 0.890 | 0.682 | 20.472 | 0.920 | 0.651 | 18.643 | 0.952 | 0.144 | 0.917 |
| 32 | 0.960 | 0.663 | 19.322 | 0.936 | 1.181 | 61.357 | 0.882 | 0.758 | 25.283 | 0.906 | 0.667 | 19.585 | 0.954 | 0.152 | 1.023 |
| 33 | 0.929 | 0.765 | 25.751 | 0.947 | 1.124 | 55.595 | 0.882 | 0.688 | 20.813 | 0.880 | 0.745 | 24.453 | 0.955 | 0.137 | 0.823 |
| 34 | 0.938 | 0.695 | 21.241 | 0.938 | 1.156 | 58.846 | 0.906 | 0.627 | 17.279 | 0.904 | 0.651 | 18.645 | 0.949 | 0.141 | 0.876 |
| 35 | 0.943 | 0.732 | 23.570 | 0.947 | 1.094 | 52.686 | 0.910 | 0.626 | 17.241 | 0.908 | 0.668 | 19.614 | 0.940 | 0.146 | 0.934 |
| 36 | 0.948 | 0.680 | 20.328 | 0.929 | 1.251 | 68.839 | 0.866 | 0.803 | 28.375 | 0.915 | 0.638 | 17.914 | 0.963 | 0.131 | 0.751 |
| 37 | 0.950 | 0.657 | 18.984 | 0.915 | 1.324 | 77.093 | 0.906 | 0.625 | 17.163 | 0.938 | 0.594 | 15.503 | 0.931 | 0.173 | 1.323 |
| 38 | 0.948 | 0.716 | 22.572 | 0.928 | 1.274 | 71.396 | 0.886 | 0.697 | 21.403 | 0.914 | 0.660 | 19.172 | 0.953 | 0.152 | 1.017 |
| 39 | 0.944 | 0.752 | 24.878 | 0.934 | 1.232 | 66.795 | 0.896 | 0.687 | 20.743 | 0.895 | 0.734 | 23.730 | 0.945 | 0.153 | 1.035 |
| 40 | 0.960 | 0.670 | 19.737 | 0.911 | 1.325 | 77.242 | 0.890 | 0.746 | 24.499 | 0.918 | 0.631 | 17.510 | 0.952 | 0.149 | 0.980 |
| 41 | 0.899 | 1.034 | 47.012 | 0.903 | 1.809 | 144.022 | 0.922 | 0.600 | 15.827 | 0.936 | 0.605 | 16.089 | 0.925 | 0.173 | 1.324 |
| 42 | 0.904 | 0.964 | 40.860 | 0.870 | 2.101 | 194.311 | 0.900 | 0.682 | 20.450 | 0.910 | 0.696 | 21.286 | 0.930 | 0.170 | 1.276 |
| 43 | 0.844 | 1.233 | 66.931 | 0.892 | 2.022 | 179.902 | 0.909 | 0.678 | 20.247 | 0.919 | 0.657 | 19.019 | 0.934 | 0.172 | 1.295 |


| 44 | 0.860 | 1.134 | 56.549 | 0.925 | 1.849 | 150.454 | 0.912 | 0.590 | 15.297 | 0.928 | 0.614 | 16.597 | 0.923 | 0.175 | 1.344 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 45 | 0.736 | 1.858 | 151.975 | 0.919 | 1.691 | 125.852 | 0.898 | 0.655 | 18.882 | 0.916 | 0.705 | 21.839 | 0.940 | 0.168 | 1.242 |
| 46 | 0.888 | 1.149 | 58.066 | 0.906 | 1.915 | 161.289 | 0.925 | 0.577 | 14.648 | 0.920 | 0.635 | 17.717 | 0.942 | 0.157 | 1.081 |
| 47 | 0.891 | 1.060 | 49.468 | 0.911 | 1.821 | 145.953 | 0.909 | 0.635 | 17.758 | 0.930 | 0.623 | 17.099 | 0.943 | 0.162 | 1.155 |
| 48 | 0.922 | 0.862 | 32.693 | 0.928 | 1.754 | 135.419 | 0.904 | 0.691 | 20.991 | 0.898 | 0.801 | 28.262 | 0.946 | 0.153 | 1.025 |
| 49 | 0.913 | 1.046 | 48.156 | 0.921 | 1.688 | 125.322 | 0.920 | 0.657 | 18.985 | 0.916 | 0.672 | 19.853 | 0.946 | 0.170 | 1.266 |
| 50 | 0.830 | 1.320 | 76.634 | 0.887 | 2.021 | 179.642 | 0.914 | 0.621 | 16.974 | 0.921 | 0.621 | 16.958 | 0.937 | 0.168 | 1.243 |
| 51 | 0.843 | 1.194 | 62.687 | 0.907 | 1.692 | 126.026 | 0.894 | 0.683 | 20.510 | 0.910 | 0.687 | 20.784 | 0.943 | 0.165 | 1.199 |
| 52 | 0.858 | 1.076 | 50.940 | 0.898 | 2.006 | 177.099 | 0.895 | 0.758 | 25.295 | 0.925 | 0.660 | 19.190 | 0.942 | 0.158 | 1.099 |
| 53 | 0.914 | 0.967 | 41.186 | 0.907 | 1.919 | 162.105 | 0.906 | 0.655 | 18.850 | 0.937 | 0.588 | 15.229 | 0.939 | 0.175 | 1.347 |
| 54 | 0.930 | 0.909 | 36.345 | 0.839 | 2.266 | 225.860 | 0.922 | 0.618 | 16.779 | 0.921 | 0.659 | 19.116 | 0.932 | 0.164 | 1.177 |
| 55 | 0.866 | 1.290 | 73.257 | 0.928 | 1.744 | 133.781 | 0.901 | 0.647 | 18.415 | 0.930 | 0.603 | 16.002 | 0.928 | 0.178 | 1.389 |
| 56 | 0.912 | 0.928 | 37.875 | 0.921 | 1.649 | 119.675 | 0.902 | 0.675 | 20.077 | 0.947 | 0.552 | 13.402 | 0.930 | 0.165 | 1.195 |
| 57 | 0.875 | 1.105 | 53.734 | 0.901 | 1.885 | 156.298 | 0.886 | 0.721 | 22.892 | 0.898 | 0.736 | 23.855 | 0.948 | 0.166 | 1.216 |
| 58 | 0.901 | 0.959 | 40.490 | 0.906 | 1.760 | 136.359 | 0.91 | 0.677 | 20.172 | 0.917 | 0.633 | 17.627 | 0.949 | 0.160 | 1.130 |
| 59 | 0.889 | 1.090 | 52.285 | 0.921 | 1.757 | 135.829 | 0.898 | 0.699 | 21.480 | 0.892 | 0.725 | 23.100 | 0.942 | 0.150 | 0.987 |
| 60 | 0.894 | 1.083 | 51.569 | 0.883 | 1.986 | 173.541 | 0.902 | 0.684 | 20.608 | 0.915 | 0.644 | 18.260 | 0.963 | 0.128 | 0.720 |
| 61 | 0.935 | 0.776 | 26.518 | 0.902 | 1.614 | 114.618 | 0.782 | 0.643 | 18.219 | 0.848 | 0.607 | 16.217 | 0.880 | 0.196 | 1.683 |
| 62 | 0.940 | 0.775 | 26.461 | 0.920 | 1.349 | 80.076 | 0.812 | 0.625 | 17.185 | 0.808 | 0.662 | 19.259 | 0.902 | 0.167 | 1.224 |
| 63 | 0.951 | 0.719 | 22.765 | 0.926 | 1.307 | 75.107 | 0.78 | 0.725 | 23.097 | 0.865 | 0.582 | 14.901 | 0.906 | 0.168 | 1.242 |
| 64 | 0.949 | 0.694 | 21.163 | 0.910 | 1.372 | 82.850 | 0.847 | 0.550 | 13.321 | 0.824 | 0.609 | 16.314 | 0.865 | 0.200 | 1.759 |
| 65 | 0.939 | 0.744 | 24.360 | 0.923 | 1.319 | 76.594 | 0.74 | 0.718 | 22.708 | 0.815 | 0.661 | 19.236 | 0.916 | 0.155 | 1.064 |
| 66 | 0.940 | 0.774 | 26.383 | 0.919 | 1.396 | 85.701 | 0.776 | 0.623 | 17.104 | 0.776 | 0.654 | 18.841 | 0.915 | 0.171 | 1.286 |
| 67 | 0.915 | 0.879 | 33.981 | 0.924 | 1.353 | 80.514 | 0.782 | 0.621 | 16.953 | 0.852 | 0.631 | 17.524 | 0.879 | 0.185 | 1.513 |
| 68 | 0.947 | 0.712 | 22.299 | 0.921 | 1.357 | 81.027 | 0.809 | 0.645 | 18.287 | 0.831 | 0.609 | 16.302 | 0.871 | 0.212 | 1.977 |
| 69 | 0.940 | 0.753 | 24.948 | 0.916 | 1.400 | 86.192 | 0.855 | 0.522 | 11.995 | 0.855 | 0.585 | 15.063 | 0.869 | 0.191 | 1.604 |
| 70 | 0.946 | 0.714 | 22.452 | 0.895 | 1.537 | 104.011 | 0.806 | 0.623 | 17.082 | 0.800 | 0.655 | 18.901 | 0.872 | 0.204 | 1.827 |
| 71 | 0.967 | 0.519 | 11.845 | 0.900 | 1.510 | 100.318 | 0.838 | 0.587 | 15.152 | 0.827 | 0.641 | 18.064 | 0.911 | 0.172 | 1.297 |
| 72 | 0.963 | 0.645 | 18.328 | 0.912 | 1.359 | 81.271 | 0.818 | 0.658 | 19.068 | 0.831 | 0.676 | 20.114 | 0.887 | 0.182 | 1.456 |
| 73 | 0.966 | 0.581 | 14.830 | 0.917 | 1.440 | 91.295 | 0.812 | 0.661 | 19.219 | 0.815 | 0.611 | 16.401 | 0.900 | 0.170 | 1.274 |
| 74 | 0.952 | 0.618 | 16.786 | 0.920 | 1.364 | 81.844 | 0.817 | 0.640 | 18.044 | 0.826 | 0.649 | 18.548 | 0.871 | 0.199 | 1.741 |
| 75 | 0.965 | 0.477 | 9.993 | 0.882 | 1.700 | 127.138 | 0.809 | 0.630 | 17.489 | 0.821 | 0.614 | 16.612 | 0.877 | 0.183 | 1.477 |
| 76 | 0.942 | 0.749 | 24.667 | 0.910 | 1.418 | 88.464 | 0.797 | 0.614 | 16.596 | 0.813 | 0.672 | 19.899 | 0.902 | 0.166 | 1.218 |
| 77 | 0.948 | 0.703 | 21.731 | 0.928 | 1.309 | 75.411 | 0.811 | 0.593 | 15.493 | 0.833 | 0.581 | 14.862 | 0.924 | 0.149 | 0.973 |
| 78 | 0.940 | 0.766 | 25.811 | 0.925 | 1.284 | 72.502 | 0.835 | 0.574 | 14.498 | 0.860 | 0.609 | 16.339 | 0.875 | 0.202 | 1.804 |
| 79 | 0.949 | 0.718 | 22.682 | 0.920 | 1.344 | 79.453 | 0.786 | 0.611 | 16.401 | 0.870 | 0.573 | 14.453 | 0.910 | 0.164 | 1.190 |
| 80 | 0.954 | 0.673 | 19.913 | 0.891 | 1.529 | 102.921 | 0.819 | 0.652 | 18.688 | 0.832 | 0.669 | 19.698 | 0.872 | 0.184 | 1.483 |
| 81 | 0.940 | 0.756 | 25.155 | 0.937 | 1.090 | 52.275 | 0.794 | 0.658 | 19.073 | 0.859 | 0.547 | 13.143 | 0.917 | 0.163 | 1.165 |
| 82 | 0.943 | 0.662 | 19.282 | 0.946 | 1.050 | 48.492 | 0.782 | 0.607 | 16.205 | 0.806 | 0.647 | 18.395 | 0.906 | 0.170 | 1.275 |
| 83 | 0.945 | 0.739 | 24.000 | 0.920 | 1.312 | 75.716 | 0.828 | 0.605 | 16.098 | 0.825 | 0.594 | 15.543 | 0.934 | 0.143 | 0.900 |
| 84 | 0.938 | 0.845 | 31.423 | 0.940 | 1.062 | 49.630 | 0.856 | 0.570 | 14.315 | 0.854 | 0.562 | 13.902 | 0.899 | 0.174 | 1.332 |
| 85 | 0.936 | 0.750 | 24.723 | 0.905 | 1.395 | 85.673 | 0.846 | 0.593 | 15.452 | 0.843 | 0.634 | 17.712 | 0.867 | 0.190 | 1.587 |
| 86 | 0.955 | 0.627 | 17.322 | 0.904 | 1.363 | 81.780 | 0.841 | 0.567 | 14.128 | 0.842 | 0.589 | 15.280 | 0.877 | 0.192 | 1.619 |
| 87 | 0.892 | 0.873 | 33.543 | 0.942 | 1.030 | 46.658 | 0.810 | 0.627 | 17.322 | 0.866 | 0.603 | 16.012 | 0.892 | 0.184 | 1.497 |
| 88 | 0.955 | 0.678 | 20.209 | 0.950 | 1.002 | 44.170 | 0.836 | 0.660 | 19.170 | 0.810 | 0.683 | 20.537 | 0.895 | 0.180 | 1.425 |
| 89 | 0.953 | 0.662 | 19.285 | 0.910 | 1.275 | 71.516 | 0.764 | 0.608 | 16.261 | 0.813 | 0.643 | 18.193 | 0.908 | 0.164 | 1.183 |
| 90 | 0.951 | 0.678 | 20.212 | 0.927 | 1.230 | 66.557 | 0.845 | 0.568 | 14.211 | 0.846 | 0.568 | 14.219 | 0.819 | 0.212 | 1.974 |


| 91 | 0.955 | 0.658 | 19.038 | 0.926 | 1.264 | 70.325 | 0.821 | 0.640 | 18.007 | 0.750 | 0.779 | 26.678 | 0.915 | 0.181 | 1.443 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 92 | 0.958 | 0.604 | 16.072 | 0.898 | 1.362 | 81.573 | 0.786 | 0.667 | 19.603 | 0.817 | 0.663 | 19.354 | 0.916 | 0.183 | 1.468 |
| 93 | 0.960 | 0.656 | 18.913 | 0.936 | 1.201 | 63.463 | 0.807 | 0.646 | 18.347 | 0.826 | 0.665 | 19.456 | 0.914 | 0.172 | 1.308 |
| 94 | 0.956 | 0.603 | 16.008 | 0.935 | 1.161 | 59.274 | 0.731 | 0.739 | 24.025 | 0.754 | 0.783 | 27.005 | 0.937 | 0.170 | 1.269 |
| 95 | 0.941 | 0.712 | 22.287 | 0.936 | 1.125 | 55.720 | 0.749 | 0.682 | 20.483 | 0.834 | 0.630 | 17.479 | 0.909 | 0.191 | 1.613 |
| 96 | 0.956 | 0.667 | 19.563 | 0.945 | 1.070 | 50.375 | 0.807 | 0.659 | 19.082 | 0.803 | 0.708 | 22.080 | 0.887 | 0.189 | 1.568 |
| 97 | 0.955 | 0.675 | 20.077 | 0.927 | 1.205 | 63.906 | 0.788 | 0.671 | 19.807 | 0.812 | 0.695 | 21.282 | 0.933 | 0.175 | 1.354 |
| 98 | 0.954 | 0.693 | 21.118 | 0.935 | 1.207 | 64.094 | 0.787 | 0.633 | 17.629 | 0.780 | 0.739 | 24.005 | 0.908 | 0.191 | 1.609 |
| 99 | 0.957 | 0.614 | 16.602 | 0.930 | 1.117 | 54.943 | 0.811 | 0.602 | 15.939 | 0.797 | 0.699 | 21.516 | 0.902 | 0.180 | 1.420 |
| 100 | 0.957 | 0.652 | 18.723 | 0.930 | 1.154 | 58.575 | 0.826 | 0.639 | 17.977 | 0.821 | 0.700 | 21.542 | 0.900 | 0.181 | 1.442 |

Note: Bold text represents an optimum number of neurons for respective response variables
Table: Statistical results obtained from ANN modelling for different response variables at a
different number of hidden neurons for k -fold cross validation method

| No. of neurons | Shelling efficiency, \% |  |  | Dehusking efficiency, \% |  |  | Germination percentage, \% |  |  | Seed coat damage, \% |  |  | Broken grain losses, \% |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{R}^{2}$ | RMSE | SSE | $\mathbf{R}^{2}$ | RMSE | SSE | $\mathbf{R}^{2}$ | RMSE | SSE | $\mathrm{R}^{2}$ | RMSE | SSE | $\mathrm{R}^{2}$ | RMSE | SSE |
| 2 | 0.763 | 1.180 | 66.802 | 0.917 | 1.270 | 77.474 | 0.716 | 0.752 | 27.152 | 0.751 | 0.746 | 26.748 | 0.740 | 0.283 | 3.837 |
| 3 | 0.828 | 0.946 | 42.995 | 0.876 | 1.415 | 96.043 | 0.832 | 0.583 | 16.329 | 0.838 | 0.619 | 18.379 | 0.871 | 0.186 | 1.653 |
| 4 | 0.882 | 0.785 | 29.569 | 0.887 | 1.353 | 87.810 | 0.832 | 0.582 | 16.261 | 0.838 | 0.618 | 18.333 | 0.867 | 0.188 | 1.702 |
| 5 | 0.927 | 0.653 | 20.455 | 0.955 | 0.934 | 41.877 | 0.787 | 0.652 | 20.409 | 0.810 | 0.653 | 20.445 | 0.877 | 0.195 | 1.820 |
| 6 | 0.936 | 0.611 | 17.947 | 0.965 | 0.821 | 32.370 | 0.786 | 0.653 | 20.443 | 0.808 | 0.656 | 20.685 | 0.875 | 0.196 | 1.836 |
| 7 | 0.931 | 0.638 | 19.558 | 0.967 | 0.805 | 31.099 | 0.784 | 0.656 | 20.643 | 0.805 | 0.660 | 20.936 | 0.869 | 0.201 | 1.938 |
| 8 | 0.934 | 0.624 | 18.697 | 0.965 | 0.829 | 33.004 | 0.827 | 0.587 | 16.559 | 0.845 | 0.589 | 16.629 | 0.894 | 0.180 | 1.563 |
| 9 | 0.941 | 0.589 | 16.630 | 0.963 | 0.851 | 34.755 | 0.857 | 0.533 | 13.649 | 0.874 | 0.531 | 13.559 | 0.932 | 0.144 | 0.996 |
| 10 | 0.933 | 0.629 | 19.019 | 0.966 | 0.814 | 31.814 | 0.890 | 0.468 | 10.500 | 0.902 | 0.469 | 10.566 | 0.903 | 0.173 | 1.431 |
| 11 | 0.930 | 0.683 | 22.389 | 0.956 | 0.976 | 45.726 | 0.910 | 0.421 | 8.507 | 0.923 | 0.417 | 8.357 | 0.948 | 0.114 | 0.622 |
| 12 | 0.928 | 0.693 | 23.023 | 0.949 | 1.051 | 52.998 | 0.928 | 0.375 | 6.747 | 0.938 | 0.373 | 6.683 | 0.904 | 0.155 | 1.154 |
| 13 | 0.940 | 0.635 | 19.328 | 0.944 | 1.092 | 57.246 | 0.925 | 0.384 | 7.070 | 0.934 | 0.385 | 7.108 | 0.934 | 0.128 | 0.786 |
| 14 | 0.926 | 0.703 | 23.696 | 0.955 | 0.982 | 46.320 | 0.933 | 0.363 | 6.331 | 0.941 | 0.366 | 6.442 | 0.959 | 0.101 | 0.488 |
| 15 | 0.920 | 0.733 | 25.782 | 0.954 | 0.994 | 47.379 | 0.944 | 0.333 | 5.308 | 0.952 | 0.328 | 5.168 | 0.969 | 0.089 | 0.378 |
| 16 | 0.925 | 0.706 | 23.920 | 0.955 | 0.979 | 45.998 | 0.938 | 0.350 | 5.886 | 0.945 | 0.352 | 5.940 | 0.960 | 0.100 | 0.484 |
| 17 | 0.939 | 0.526 | 13.286 | 0.855 | 1.574 | 118.846 | 0.850 | 0.445 | 9.491 | 0.853 | 0.471 | 10.649 | 0.884 | 0.165 | 1.307 |
| 18. | 0.942 | 0.621 | 18.531 | 0.959 | 0.940 | 42.384 | 0.941 | 0.341 | 5.585 | 0.948 | 0.342 | 5.603 | 0.951 | 0.110 | 0.586 |
| 19. | 0.924 | 0.637 | 19.447 | 0.907 | 1.281 | 78.786 | 0.846 | 0.566 | 15.373 | 0.864 | 0.569 | 15.565 | 0.937 | 0.135 | 0.874 |
| 20 | 0.942 | 0.622 | 18.577 | 0.957 | 0.959 | 44.117 | 0.917 | 0.403 | 7.783 | 0.926 | 0.409 | 8.048 | 0.952 | 0.109 | 0.571 |
| 21 | 0.934 | 0.664 | 21.191 | 0.961 | 0.912 | 39.960 | 0.943 | 0.333 | 5.328 | 0.949 | 0.338 | 5.481 | 0.957 | 0.104 | 0.514 |
| 22 | 0.943 | 0.618 | 18.334 | 0.959 | 0.942 | 42.582 | 0.929 | 0.373 | 6.681 | 0.939 | 0.372 | 6.634 | 0.959 | 0.101 | 0.486 |
| 23 | 0.942 | 0.624 | 18.712 | 0.954 | 0.992 | 47.248 | 0.927 | 0.378 | 6.862 | 0.935 | 0.383 | 7.040 | 0.955 | 0.106 | 0.541 |
| 24 | 0.947 | 0.596 | 17.039 | 0.955 | 0.986 | 46.679 | 0.934 | 0.359 | 6.177 | 0.942 | 0.362 | 6.277 | 0.964 | 0.095 | 0.434 |
| 25 | 0.932 | 0.555 | 14.760 | 0.875 | 1.464 | 102.935 | 0.843 | 0.455 | 9.953 | 0.853 | 0.472 | 10.676 | 0.896 | 0.156 | 1.172 |
| 26 | 0.941 | 0.628 | 18.919 | 0.954 | 0.994 | 47.450 | 0.939 | 0.347 | 5.770 | 0.947 | 0.347 | 5.783 | 0.962 | 0.098 | 0.460 |
| 27 | 0.922 | 0.644 | 19.931 | 0.913 | 1.237 | 73.412 | 0.809 | 0.630 | 19.047 | 0.832 | 0.633 | 19.249 | 0.922 | 0.150 | 1.081 |
| 28 | 0.941 | 0.626 | 18.838 | 0.957 | 0.956 | 43.904 | 0.945 | 0.329 | 5.209 | 0.951 | 0.332 | 5.295 | 0.960 | 0.100 | 0.479 |
| 29 | 0.929 | 0.615 | 18.156 | 0.914 | 1.231 | 72.737 | 0.826 | 0.601 | 17.340 | 0.850 | 0.599 | 17.223 | 0.919 | 0.153 | 1.130 |
| 30 | 0.925 | 0.709 | 24.150 | 0.956 | 0.971 | 45.211 | 0.936 | 0.354 | 6.011 | 0.944 | 0.355 | 6.052 | 0.966 | 0.092 | 0.403 |
| 31 | 0.939 | 0.636 | 19.427 | 0.959 | 0.936 | 42.037 | 0.932 | 0.365 | 6.381 | 0.940 | 0.368 | 6.486 | 0.962 | 0.097 | 0.450 |
| 32 | 0.953 | 0.559 | 14.993 | 0.961 | 0.919 | 40.533 | 0.940 | 0.344 | 5.696 | 0.948 | 0.343 | 5.660 | 0.964 | 0.095 | 0.434 |


| 33 | 0.935 | 0.661 | 20.960 | 0.959 | 0.937 | 42.121 | 0.938 | 0.348 | 5.813 | 0.946 | 0.349 | 5.846 | 0.951 | 0.110 | 0.583 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 34 | 0.941 | 0.629 | 19.006 | 0.961 | 0.920 | 40.589 | 0.950 | 0.314 | 4.747 | 0.956 | 0.317 | 4.821 | 0.962 | 0.097 | 0.453 |
| 35 | 0.948 | 0.589 | 16.632 | 0.952 | 1.019 | 49.880 | 0.961 | 0.277 | 3.691 | 0.965 | 0.280 | 3.754 | 0.963 | 0.096 | 0.443 |
| 36 | 0.935 | 0.588 | 16.608 | 0.840 | 1.681 | 135.605 | 0.823 | 0.607 | 17.658 | 0.845 | 0.609 | 17.827 | 0.915 | 0.157 | 1.183 |
| 37 | 0.952 | 0.566 | 15.366 | 0.961 | 0.914 | 40.130 | 0.952 | 0.308 | 4.558 | 0.957 | 0.312 | 4.661 | 0.975 | 0.079 | 0.300 |
| 38 | 0.949 | 0.583 | 16.320 | 0.956 | 0.969 | 45.030 | 0.955 | 0.297 | 4.247 | 0.961 | 0.296 | 4.202 | 0.975 | 0.079 | 0.299 |
| 39 | 0.933 | 0.553 | 14.672 | 0.900 | 1.308 | 82.164 | 0.875 | 0.405 | 7.885 | 0.883 | 0.421 | 8.498 | 0.912 | 0.144 | 1.000 |
| 40 | 0.958 | 0.532 | 13.592 | 0.962 | 0.903 | 39.100 | 0.959 | 0.283 | 3.838 | 0.965 | 0.283 | 3.851 | 0.973 | 0.083 | 0.328 |
| 41 | 0.958 | 0.470 | 10.623 | 0.978 | 0.644 | 19.938 | 0.946 | 0.324 | 5.043 | 0.952 | 0.327 | 5.118 | 0.964 | 0.105 | 0.525 |
| 42 | 0.959 | 0.462 | 10.261 | 0.978 | 0.642 | 19.804 | 0.940 | 0.344 | 5.664 | 0.946 | 0.348 | 5.797 | 0.971 | 0.093 | 0.416 |
| 43 | 0.947 | 0.618 | 18.318 | 0.981 | 0.651 | 20.329 | 0.928 | 0.392 | 7.371 | 0.937 | 0.393 | 7.416 | 0.984 | 0.069 | 0.230 |
| 44 | 0.912 | 0.610 | 17.866 | 0.687 | 2.161 | 224.065 | 0.819 | 0.570 | 15.571 | 0.825 | 0.597 | 17.130 | 0.736 | 0.253 | 3.065 |
| 45 | 0.914 | 0.603 | 17.455 | 0.578 | 2.510 | 302.323 | 0.733 | 0.692 | 22.974 | 0.740 | 0.728 | 25.430 | 0.776 | 0.233 | 2.601 |
| 46 | 0.947 | 0.617 | 18.279 | 0.983 | 0.622 | 18.572 | 0.932 | 0.380 | 6.918 | 0.941 | 0.380 | 6.918 | 0.987 | 0.063 | 0.188 |
| 47 | 0.955 | 0.488 | 11.438 | 0.964 | 0.831 | 33.139 | 0.925 | 0.383 | 7.028 | 0.937 | 0.375 | 6.764 | 0.974 | 0.088 | 0.371 |
| 48 | 0.933 | 0.592 | 16.845 | 0.965 | 0.813 | 31.749 | 0.929 | 0.373 | 6.680 | 0.933 | 0.386 | 7.153 | 0.974 | 0.089 | 0.380 |
| 49 | 0.950 | 0.514 | 12.658 | 0.964 | 0.832 | 33.208 | 0.931 | 0.366 | 6.437 | 0.944 | 0.356 | 6.069 | 0.976 | 0.086 | 0.355 |
| 50 | 0.953 | 0.495 | 11.766 | 0.966 | 0.800 | 30.734 | 0.933 | 0.362 | 6.289 | 0.946 | 0.348 | 5.813 | 0.971 | 0.094 | 0.426 |
| 51 | 0.946 | 0.531 | 13.551 | 0.960 | 0.872 | 36.538 | 0.929 | 0.373 | 6.666 | 0.938 | 0.373 | 6.664 | 0.973 | 0.090 | 0.386 |
| 52 | 0.953 | 0.499 | 11.937 | 0.964 | 0.822 | 32.467 | 0.942 | 0.335 | 5.396 | 0.948 | 0.341 | 5.598 | 0.975 | 0.087 | 0.362 |
| 53 | 0.944 | 0.635 | 19.378 | 0.969 | 0.845 | 34.276 | 0.921 | 0.409 | 8.018 | 0.932 | 0.407 | 7.944 | 0.985 | 0.066 | 0.209 |
| 54 | 0.955 | 0.487 | 11.369 | 0.969 | 0.765 | 28.127 | 0.940 | 0.342 | 5.600 | 0.942 | 0.360 | 6.235 | 0.974 | 0.089 | 0.376 |
| 55 | 0.936 | 0.521 | 13.041 | 0.801 | 1.725 | 142.874 | 0.808 | 0.587 | 16.553 | 0.807 | 0.627 | 18.869 | 0.812 | 0.213 | 2.185 |
| 56 | 0.948 | 0.522 | 13.059 | 0.967 | 0.788 | 29.835 | 0.929 | 0.373 | 6.663 | 0.938 | 0.374 | 6.697 | 0.975 | 0.087 | 0.361 |
| 57 | 0.918 | 0.658 | 20.774 | 0.958 | 0.891 | 38.089 | 0.919 | 0.397 | 7.568 | 0.925 | 0.409 | 8.035 | 0.966 | 0.102 | 0.500 |
| 58 | 0.910 | 0.615 | 18.181 | 0.751 | 1.927 | 178.323 | 0.818 | 0.571 | 15.637 | 0.817 | 0.610 | 17.889 | 0.772 | 0.235 | 2.650 |
| 59 | 0.952 | 0.504 | 12.188 | 0.963 | 0.836 | 33.534 | 0.936 | 0.353 | 5.982 | 0.944 | 0.354 | 6.006 | 0.975 | 0.086 | 0.359 |
| 60 | 0.896 | 0.663 | 21.093 | 0.723 | 2.033 | 198.387 | 0.796 | 0.606 | 17.603 | 0.817 | 0.611 | 17.890 | 0.755 | 0.244 | 2.848 |
| 61 | 0.924 | 0.654 | 20.534 | 0.983 | 0.612 | 17.960 | 0.919 | 0.384 | 7.086 | 0.925 | 0.397 | 7.574 | 0.973 | 0.085 | 0.344 |
| 62 | 0.952 | 0.474 | 10.789 | 0.940 | 0.908 | 39.543 | 0.894 | 0.400 | 7.695 | 0.910 | 0.398 | 7.614 | 0.949 | 0.105 | 0.531 |
| 63 | 0.960 | 0.436 | 9.108 | 0.949 | 0.837 | 33.621 | 0.912 | 0.366 | 6.434 | 0.927 | 0.358 | 6.162 | 0.967 | 0.085 | 0.345 |
| 64 | 0.892 | 0.778 | 29.088 | 0.961 | 0.911 | 39.846 | 0.895 | 0.437 | 9.152 | 0.898 | 0.463 | 10.288 | 0.962 | 0.101 | 0.487 |
| 65 | 0.925 | 0.651 | 20.427 | 0.984 | 0.586 | 17.857 | 0.919 | 0.384 | 7.089 | 0.932 | 0.377 | 6.716 | 0.971 | 0.088 | 0.343 |
| 66 | 0.959 | 0.436 | 9.195 | 0.941 | 0.892 | 39.109 | 0.899 | 0.396 | 7.372 | 0.914 | 0.464 | 7.305 | 0.966 | 0.350 | 0.391 |
| 67 | 0.957 | 0.449 | 9.667 | 0.945 | 0.872 | 36.459 | 0.904 | 0.382 | 7.019 | 0.919 | 0.379 | 6.887 | 0.966 | 0.086 | 0.353 |
| 68 | 0.917 | 0.683 | 22.396 | 0.980 | 0.658 | 20.784 | 0.918 | 0.387 | 7.171 | 0.916 | 0.420 | 8.485 | 0.972 | 0.087 | 0.361 |
| 69 | 0.919 | 0.676 | 21.930 | 0.978 | 0.693 | 23.025 | 0.923 | 0.374 | 6.730 | 0.932 | 0.379 | 6.899 | 0.972 | 0.086 | 0.355 |
| 70 | 0.950 | 0.486 | 11.340 | 0.938 | 0.920 | 40.657 | 0.904 | 0.382 | 7.003 | 0.908 | 0.402 | 7.767 | 0.956 | 0.098 | 0.457 |
| 71 | 0.893 | 0.781 | 29.310 | 0.942 | 1.085 | 56.494 | 0.917 | 0.399 | 7.638 | 0.941 | 0.357 | 6.109 | 0.971 | 0.086 | 0.354 |
| 72 | 0.924 | 0.661 | 20.984 | 0.958 | 0.927 | 41.281 | 0.961 | 0.273 | 3.570 | 0.961 | 0.291 | 4.071 | 0.977 | 0.076 | 0.276 |
| 73 | 0.919 | 0.681 | 22.229 | 0.956 | 0.945 | 42.846 | 0.956 | 0.289 | 4.003 | 0.964 | 0.278 | 3.709 | 0.978 | 0.074 | 0.264 |
| 74 | 0.919 | 0.683 | 22.383 | 0.956 | 0.945 | 42.856 | 0.960 | 0.276 | 3.656 | 0.964 | 0.279 | 3.737 | 0.979 | 0.074 | 0.260 |
| 75 | 0.952 | 0.522 | 13.095 | 0.960 | 0.901 | 38.931 | 0.959 | 0.278 | 3.717 | 0.963 | 0.283 | 3.831 | 0.977 | 0.076 | 0.275 |
| 76 | 0.901 | 0.755 | 27.345 | 0.942 | 1.085 | 56.504 | 0.934 | 0.356 | 6.097 | 0.937 | 0.370 | 6.587 | 0.976 | 0.079 | 0.297 |
| 77 | 0.900 | 0.757 | 27.493 | 0.941 | 1.100 | 58.065 | 0.910 | 0.416 | 8.294 | 0.927 | 0.397 | 7.582 | 0.975 | 0.079 | 0.300 |
| 78 | 0.937 | 0.600 | 17.286 | 0.953 | 0.978 | 45.898 | 0.957 | 0.286 | 3.926 | 0.960 | 0.293 | 4.116 | 0.978 | 0.074 | 0.262 |
| 79 | 0.897 | 0.769 | 28.420 | 0.949 | 1.021 | 50.067 | 0.919 | 0.393 | 7.408 | 0.936 | 0.373 | 6.688 | 0.973 | 0.082 | 0.323 |


| 80 | 0.907 | 0.729 | 25.501 | 0.948 | 1.030 | 50.959 | 0.930 | 0.366 | 6.430 | 0.924 | 0.407 | 7.963 | 0.977 | 0.076 | 0.276 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 81 | 0.952 | 0.524 | 13.164 | 0.962 | 0.883 | 37.414 | 0.961 | 0.273 | 3.580 | 0.967 | 0.267 | 3.424 | 0.979 | 0.073 | 0.259 |
| 82 | 0.942 | 0.579 | 16.077 | 0.958 | 0.930 | 41.497 | 0.963 | 0.265 | 3.381 | 0.968 | 0.265 | 3.378 | 0.978 | 0.074 | 0.261 |
| 83 | 0.961 | 0.476 | 10.863 | 0.961 | 0.855 | 35.120 | 0.963 | 0.290 | 4.044 | 0.967 | 0.293 | 4.112 | 0.962 | 0.107 | 0.545 |
| 84 | 0.927 | 0.648 | 20.125 | 0.958 | 0.927 | 41.220 | 0.960 | 0.275 | 3.632 | 0.965 | 0.275 | 3.627 | 0.978 | 0.075 | 0.269 |
| 85 | 0.951 | 0.535 | 13.723 | 0.956 | 0.907 | 39.506 | 0.945 | 0.352 | 5.936 | 0.956 | 0.337 | 5.437 | 0.957 | 0.114 | 0.621 |
| 86 | 0.906 | 0.733 | 25.811 | 0.948 | 1.034 | 51.352 | 0.919 | 0.394 | 7.453 | 0.933 | 0.380 | 6.940 | 0.967 | 0.091 | 0.398 |
| 87 | 0.898 | 0.766 | 28.198 | 0.947 | 1.044 | 52.288 | 0.948 | 0.317 | 4.811 | 0.954 | 0.317 | 4.813 | 0.973 | 0.083 | 0.330 |
| 88 | 0.934 | 0.613 | 18.037 | 0.959 | 0.911 | 39.826 | 0.962 | 0.269 | 3.465 | 0.967 | 0.267 | 3.418 | 0.979 | 0.073 | 0.257 |
| 89 | 0.917 | 0.690 | 22.850 | 0.946 | 1.047 | 52.619 | 0.925 | 0.380 | 6.915 | 0.935 | 0.376 | 6.799 | 0.973 | 0.083 | 0.332 |
| 90 | 0.931 | 0.627 | 18.893 | 0.957 | 0.932 | 41.711 | 0.961 | 0.273 | 3.583 | 0.965 | 0.276 | 3.645 | 0.978 | 0.075 | 0.269 |
| 91 | 0.847 | 0.900 | 38.840 | 0.939 | 1.122 | 60.394 | 0.863 | 0.557 | 14.911 | 0.880 | 0.559 | 15.006 | 0.953 | 0.126 | 0.763 |
| 92 | 0.961 | 0.476 | 10.871 | 0.923 | 1.119 | 60.053 | 0.889 | 0.454 | 9.911 | 0.899 | 0.463 | 10.279 | 0.922 | 0.139 | 0.933 |
| 93 | 0.959 | 0.485 | 11.288 | 0.922 | 1.126 | 60.876 | 0.877 | 0.478 | 10.964 | 0.887 | 0.489 | 11.491 | 0.924 | 0.138 | 0.908 |
| 94 | 0.961 | 0.473 | 10.756 | 0.923 | 1.122 | 60.458 | 0.885 | 0.462 | 10.256 | 0.888 | 0.487 | 11.399 | 0.925 | 0.136 | 0.892 |
| 95 | 0.960 | 0.480 | 11.046 | 0.928 | 1.086 | 56.622 | 0.887 | 0.459 | 10.101 | 0.896 | 0.470 | 10.609 | 0.925 | 0.136 | 0.893 |
| 96 | 0.960 | 0.478 | 10.963 | 0.922 | 1.126 | 60.815 | 0.891 | 0.452 | 9.790 | 0.896 | 0.470 | 10.622 | 0.925 | 0.137 | 0.897 |
| 97 | 0.960 | 0.480 | 11.039 | 0.921 | 1.131 | 61.444 | 0.871 | 0.490 | 11.502 | 0.873 | 0.519 | 12.945 | 0.924 | 0.137 | 0.903 |
| 98 | 0.960 | 0.479 | 11.028 | 0.918 | 1.159 | 64.519 | 0.877 | 0.479 | 10.995 | 0.877 | 0.511 | 12.550 | 0.924 | 0.137 | 0.902 |
| 99 | 0.959 | 0.485 | 11.273 | 0.924 | 1.110 | 59.149 | 0.888 | 0.457 | 10.012 | 0.896 | 0.471 | 10.633 | 0.925 | 0.137 | 0.895 |
| 100 | 0.960 | 0.479 | 10.992 | 0.926 | 1.096 | 57.677 | 0.889 | 0.454 | 9.911 | 0.892 | 0.478 | 10.987 | 0.926 | 0.136 | 0.885 |

