# Optimality and Efficiency of Neighbouring Design 

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#### Abstract

SUMMARY This paper deals with the optimality and efficiency of Nearest Neighbour Balanced Block Designs (NNBD) using Generalised Least Square method of estimation for different correlated models (AR(1), AR(2), MA(1), MA(2) and ARMA (1, 1)). NNBD turns out to be optimal for AR(1) model and the performance of NNBD is quite satisfactory for the remaining models. The efficiency of the proposed design in comparison to regular block design is substantial for the above correlated models.


Key words: Auto-regressive model, Moving average model, ARMA model, Correlated errors, Generalised least square estimation, Optimality and efficiency.

## 1. Introduction

In the analysis of the comparative experiments, it is usually assumed that the observations are independently distributed. The usual methods of local control adopted in comparative experiments such as randomized block design, latin square, BIBD and PBIBD serve the purpose well, when fertility variation is smooth and well known. These methods perform poorly in more realistic situations where fertility variation changes in an unknown fashion. Under these circumstances, it may be useful to adjust for fertility in a more continuous manner such as making use of the inter-dependence among neighbouring observations (Gill and Shukla, [31).

Usually in comparative experiments the treatments are allocated at random to plots within a block ignoring the order of allocation of the treatments. However in neighbour design the ordering of treatments with in blocks and number of times that any two treatments appear in adjacent plots within block are important. These designs are known as one dimensional designs. These designs may be block designs in which the neighbours of a given plot are those of the immediate left and right.

[^0]Street and Street [9] has considered the use of BIBD (one dimensional NNBIBD) for use in seed orchards with $t=$ (a prime number) of form $6 u+1$, ( $u$ is a non negative integer), $b, k, r$ and $\lambda$ are the parameters. Universal optimality of NNBD using ARMA models has been introduced by Santharam and Ponuuswamy [8]. Efficiencies of NNBD using ARMA models have also been studied by Santharam and Ponnuswamy [8].

In the present paper, we have taken NNBD with the parameter stucture $t=5, b=5, k=5, r=5, \lambda=1$ and investigated the optimality and efficiency of NNBD for

$$
\rho=0.1(0.1) 0.9 \quad \text { and } \quad\left(\rho_{1}, \rho_{2}\right)=(.1, .1),(.2, .2) \ldots(.9, .9)
$$

(where $\rho_{1}, \rho_{2}$ and $\rho$ are the correlation coefficients) when errors behave according to AR(1), MA(1), ARMA (1, 1), AR(2) and MA(2) models.

## 2. Universal Optimality

Keifer [5] introduced the universal optimality criterion which includes the well known D, A and E optimality criteria as special cases. The sufficient conditions for a design $\mathrm{d}^{*}$ in $\Delta$ (where $\Delta$ is a class of unary block designs) to be universally optimal are:
(i) the matrix $\mathrm{C}_{\mathrm{d}}^{*}$ is completely symmetric in the sense that all the diagonal elements are the same and all the off diagonal elements are the same.
(ii) $\operatorname{tr}\left(C_{d}^{*}\right) \geq \operatorname{tr}\left(C_{d}\right)$, for all $d$ in $\Delta$

In some cases, it is not possible to find a design with specified parameters having completely symmetric information matrix. In such cases, it is expected that a design with information matrix nearly completely symmetric and satisfying condition (ii) is nearly optimal.
$\operatorname{AR}(1), \mathrm{MA}(1)$, and $\operatorname{ARMA}(1,1)$ in
Nearest Neighbour Balanced Block Design (NNBD)
Let $\Delta$ be a class of mary block designs for $t$ treatments in which each treatment is applied to r plots, the tr plots being arranged in b blocks, each $k \leq t$, let $y$ be a $t r \times 1$ random vector corresponding to the observations. Consider a fixed effect additive linear model

$$
\begin{equation*}
y=X \tau+Z \beta+\varepsilon+\eta \tag{1}
\end{equation*}
$$

where X is the observation-tratment incidence matrix of order $\mathrm{tr} \times \mathrm{t} ; \mathrm{Z}$ is the observation-block incidence matrix of order $\mathrm{tr} \times \mathrm{b} ; \tau$ and $\beta$ are vectors of
treatment and block effects, respectively: $\varepsilon$ is a random error vector representing local variation in soil fertility with $E(\varepsilon)=0$ and $\operatorname{Var}(\varepsilon)=\sigma_{\varepsilon}^{2} \Omega: \eta$ is an additional error vector with $\mathrm{E}(\eta)=0$ and $\operatorname{Var}(\eta)=\sigma_{\eta}^{2} \mathrm{I}$, representing other sources of variability in plots which are independent of local fertility. Therefore, $\operatorname{Var}(\mathrm{y})=\sigma_{\varepsilon}^{2} \Omega+\sigma_{\eta}^{2} \mathrm{I}=\mathrm{V}$, say.

The model (1) is called an error-in-variables model (Besag [1]) and is closely related to the smooth 'trend plus error' model of Wikinson et al. [111). This is a general model which gives a better fit in situations where the error structure is non-stationary (Besag [1]; Wilkinson et al. [11]; Patterson [6]).

The five correlation models considered for the error vector $\varepsilon$ in (1) are the first-order autoregressive model, the moving average model, autoregressive-moving average model, second order auto-regressive and moving average models.

## 3. Information Matrix

Consider the model $Y=X \tau+Z \boldsymbol{Z}+\boldsymbol{\varepsilon}+\boldsymbol{\eta}$
The generalised least squares nomal equations for estimating $\tau$ and $\beta$ are

$$
\begin{aligned}
& X^{\prime} V^{-1} X \hat{T}+X^{\prime} V^{-1} Z \hat{\beta}=X^{\prime} V^{-1} y \\
& Z^{\prime} V^{-1} X \hat{\tau}+Z^{\prime} V^{-1} Z \hat{\beta}=Z^{\prime} V^{-1} y
\end{aligned}
$$

Reduced normal equations for $\hat{\tau}$ can be written as

$$
\mathrm{C} \hat{T}=\mathrm{Qy}
$$

where

$$
C=X^{\prime} V^{-1} X-X^{\prime} V^{-1} Z\left(Z^{\prime} V^{-1} Z\right)^{-1} Z^{\prime} V^{-1}
$$

and

$$
Q=X^{\prime} V^{-1}-X^{\prime} V^{-1} Z\left(Z^{\prime} V^{-1} Z\right)^{-1} Z^{\prime} V^{-1} X
$$

The matrix $C$ (Gill and Shukla [3]) is called the information matrix of a design for treatment parameters. To emphasize the dependence of information matrix on design, we write it as $C_{d}$ for $d \in \Delta$, row sums and column sums of $C_{d}$ are zero for each $d \in \Delta$. We assume that rauk $\left(C_{d}\right)=t-1$ for each $d \in \Delta$, so that all the treatment contrasts are estimable.

## 4. Deviation from Exact Optimality

Since $\operatorname{tr}\left(C_{d}\right)$ is constant over the class $\Delta$, the departure from exact optimality of a design can be measured by the departure of $\mathrm{C}_{\mathrm{d}}$ from complete symmetry. This departure is measured by two indices $\mathrm{E}_{\mathrm{D}}$ and $\mathrm{E}_{\mathrm{A}}$ called D-efficiency and A-efficiency, respectively by Cheng and Wu [2].

Let $\gamma_{\mathrm{d} 1}, \ldots, \gamma_{\mathrm{d}, \mathrm{t}-\mathrm{l}}$ be the non-zero eigenvalues of $\mathrm{C}_{\mathrm{d}}$. The design is universally optimal if all $\gamma_{\mathrm{di}}$ 's are equal. However, such a design for a given set of parameters may not exist. The information matrix of the hypothetical optimal design would have eigenvalue $\gamma=(t-1)^{-1}\left(\gamma_{d 1}+\ldots+\gamma_{d, t-1}\right)$ with multiplicity $\mathrm{t}-1$. The product $\Pi \gamma_{\mathrm{d}}=\gamma_{\mathrm{d} 1} \ldots \gamma_{\mathrm{d}, \mathrm{t}-1}$ is maximum for this design and is equal to $\gamma^{\gamma^{-1}}$. The D-efficiency of a design d relative to the hypothetical universally optimal design can be defined as $\mathrm{E}_{\mathrm{D}}=\gamma^{-(\mathrm{t}-1)} \Pi \gamma_{\mathrm{di}}$. Similarly, the harnonic mean of the $\gamma_{\mathrm{di}}$ 's is a maximum for the hypothetical design and is equal to $\gamma$. The A-efficiency of $d$ is defined similarly by $\mathrm{E}_{\mathrm{A}}=(\mathrm{t}-1) \gamma^{-1}\left(\Sigma \gamma_{\mathrm{di}}^{-1}\right)^{-1}$.

Conversely, an inefficient design is one with highly dissimilar $\gamma_{\text {di }}$ 's. This happens when parameters $\mathrm{e}_{\mathrm{i}}, \mu_{\mathrm{ij}}$ and $\mathrm{g}_{\mathrm{ij}}$ are different to the maximum possible extent. This is the case with a regular design which has the same spatial configuration of treatments in every block. Therefore, D-efficiency and A-efficiency of a regular design are the lower bounds of the efficiencies.

Table 1 and 2 show the A-efficiency, $E_{A}$ and the D-efficiency $E_{D}$ of complete nearest neighbour block design with $t=5, r=5$ when errors behave under autoregressive, moving average and ARMA processes. These lower bounds are the respective values for regular designs with the same number of treatments and replications. The ratio $\sigma_{\eta}^{2} / \sigma_{\varepsilon}^{2}=\alpha$ takes values 0 and $\frac{1}{2}$. An empirical value of $\alpha$ obtained from a series of trials was 0.42 (Patterson [6]).

## Conclusion

In this paper we have investigated the optimality of block designs when observations within a block are assumed to be correlated and generalized least square method of estimation has been used, when the errors follow $\operatorname{AR}(1)$, MA(1), ARMA (1, 1), AR(2) and MA(2) models. The gain in efficiencies (A and D) of NNBD over regular block design is substantial for all the above models.
Table 1 : A-efficiency and D-efficiency of some nearest neighbour balanced designs ; lower bounds of efficiencies in parentheses

| ( $\mathrm{t}-5 \mathrm{r}-5$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Error Model | $\rho-0.1$ | $\rho=0.2$ |  | 0.3 |  | -0.4 |  | -0.5 |  | -0.6 |  | -0.7 |  | -0.8 |  | -0.9 |
| $\alpha=0 \alpha=.5 \alpha=0 \alpha=.5 \alpha=0 \alpha=.5 \alpha=0 \alpha=.5 \alpha=0 \alpha=.5 \alpha=0 \alpha-.5 \alpha=0 \alpha=.5 \alpha-0 \alpha=.5 \alpha=0 \alpha=.5$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AR(1) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $E_{\text {A }}$ | $\begin{array}{cc} 1.000 & 1.000 \\ (.990) & (.995) \end{array}$ | $\begin{array}{ll} 1.000 & 1.000 \\ (.961) & (.983) \end{array}$ | $\begin{array}{cc} 1.000 & 1.000 \\ (.919) & (.965) \end{array}$ |  | $\begin{array}{cc} 1.000 & 1.000 \\ (.866) & (.942) \end{array}$ |  | $\begin{array}{cc} 1.000 & 1.000 \\ (.807) & (.915) \end{array}$ |  | $\begin{array}{ll} 1.000 & 1.000 \\ (.745) & (.961) \end{array}$ |  | $\begin{array}{ll} 1.000 & 1.000 \\ (.684) & (.853) \end{array}$ |  | $\begin{array}{ll} 1.000 & 1.000 \\ (.618) & (.820) \end{array}$ |  | $\begin{array}{ll} 1.000 & 1.000 \\ (.558) & (.785) \end{array}$ |  |
| $E_{\text {D }}$ | $\begin{array}{ll} 1.000 & 1.000 \\ (.980) & (.991) \end{array}$ | $\begin{array}{ll} 1.000 & 1.000 \\ (.925) & (.967) \end{array}$ | $\begin{array}{cc} 1.000 & 1.000 \\ (.848) & (.933) \end{array}$ |  | $\begin{array}{ll} 1.000 & 1.000 \\ (.758) & (.890) \end{array}$ |  | $\begin{array}{ll} 1.000 & 1.000 \\ (.666) & (.844) \end{array}$ |  | $\begin{array}{ll} 1.000 & 1.000 \\ (.578) & (.924) \end{array}$ |  | $\begin{array}{ll} 1.000 & 1.000 \\ (.497)(.796) \end{array}$ |  | $\begin{array}{ll} 1.000 & 1.000 \\ (.497) & (.699) \end{array}$ |  | $\begin{array}{cc} 1.000 & 1.000 \\ (.364) & (.654) \end{array}$ |  |
| MA(1) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{E}_{\mathrm{A}}$ | $\begin{array}{cc} 1.000 & 1.000 \\ (.987) & (.994) \end{array}$ | $\begin{array}{ll} 0.994 & 0.998 \\ (.947) & (.978) \end{array}$ | $\begin{gathered} 0.977 \\ (.882 \end{gathered}$ | $\begin{gathered} 0.994 \\ (.950) \end{gathered}$ | $\begin{array}{cc} 0.943 & 0.986 \\ (.798) & (.913) \end{array}$ |  | $\begin{aligned} & 0.885 \\ & (.706 \end{aligned}$ | $\begin{aligned} & 0.974 \\ & (.871) \end{aligned}$ | $\begin{gathered} 0.807 \\ (.621 \end{gathered}$ | $\begin{gathered} 0.957 \\ (.828) \end{gathered}$ | $\begin{aligned} & 0.721 \\ & (.550) \end{aligned}$ | $\begin{aligned} & 0.938 \\ & (.788) \end{aligned}$ | $\begin{array}{cc} 0.647 & 0.917 \\ (.499) & (.752) \end{array}$ |  | $\begin{array}{cc} 0.598 & 0.899 \\ (.471) & (.725) \end{array}$ |  |
| $\mathrm{E}_{\mathrm{D}}$ | $\begin{array}{cc} 0.998 & 1.000 \\ (.975) & (.989) \end{array}$ | $\begin{array}{ll} 0.987 & 0.996 \\ (.898) & (.956) \end{array}$ | $\begin{array}{cc} 0.955 & 0.988 \\ (.777) & (.902 \end{array}$ |  | $\begin{array}{cc} 0.889 & 0.973 \\ (.636) & (.834) \end{array}$ |  | $\begin{array}{cl} 0.784 & 0.949 \\ (.497) & (.758) \end{array}$ |  | $\begin{gathered} 0.650 \\ (.385 \end{gathered}$ | $\begin{aligned} & 0.916 \\ & (.686) \end{aligned}$ | $\begin{array}{cc} 0.519 & 0.879 \\ (.301) & (.620) \end{array}$ |  | $\begin{gathered} 0.417 \\ (.247) \end{gathered}$ | $\frac{0.841}{(.566)}$ | $\begin{array}{cc} 0.357 & 0.809 \\ (.221) & (.525) \end{array}$ |  |
| $\begin{gathered} \text { ARMA } \\ (1,1) \end{gathered}$ | $\begin{aligned} & \rho_{1}=.1 \\ & \rho_{2}=.1 \end{aligned}$ | $\begin{aligned} & \rho_{1}=.2 \\ & \rho_{2}=.2 \end{aligned}$ | $\begin{aligned} & \rho_{1}=.3 \\ & \rho_{2}=.3 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.4 \\ & \rho_{2}=.4 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.5 \\ & \rho_{2}-.5 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.6 \\ & \rho_{2}=.6 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}-.7 \\ & \rho_{2}-.7 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.8 \\ & \rho_{2}=.8 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.9 \\ & \rho_{2}=.9 \end{aligned}$ |  |
| $\mathbf{E}_{\text {A }}$ | $\begin{array}{cc} 1.000 & 1.000 \\ (.957) & (.982) \end{array}$ | $\begin{array}{ll} 0.996 & 1.000 \\ (.841) & (.931) \end{array}$ | $\begin{array}{ll} 0.980 & 1.000 \\ (.685) & (.858) \end{array}$ |  | $\begin{array}{ll} 0.945 & 0.998 \\ (.526) & (.776) \end{array}$ |  | $\begin{aligned} & 0.888 \\ & (.392 \end{aligned}$ | $\begin{aligned} & 0.995 \\ & (.689) \end{aligned}$ | $\begin{gathered} 0.819 \\ (.287) \end{gathered}$ | $\begin{gathered} 0.993 \\ (.609) \end{gathered}$ | $0.751$ | $\begin{gathered} 0.990 \\ (.537) \end{gathered}$ | $\begin{aligned} & 0.696 \\ & (.165) \end{aligned}$ | $\begin{aligned} & 0.988 \\ & (.472) \end{aligned}$ | $\begin{aligned} & 0.661 \\ & (.133) \end{aligned}$ | $\begin{aligned} & 0.987 \\ & (.414) \end{aligned}$ |
| $\mathrm{E}_{\text {D }}$ | $\begin{array}{ll} 1.000 & 1.000 \\ (.917) & (.963) \end{array}$ | $\begin{array}{ll} 0.992 & 1.000 \\ (.707) & (.868) \end{array}$ | 0.9610 .998  <br> $(.467)$ $(.741)$ |  | $\begin{array}{ll} 0.893 & 0.995 \\ (.272) & (.611) \end{array}$ |  | $\begin{array}{cc} 0.789 & 0.991 \\ (.147) & (.491) \end{array}$ |  | $\begin{array}{ll} 0.671 & 0.986 \\ (.076) & (.392) \end{array}$ |  | $\begin{array}{ll} 0.564 & 0.981 \\ (.041) & (.317) \end{array}$ |  | $\begin{array}{cc} 0.485 & 0.977 \\ (.024) & (.257) \end{array}$ |  | $\begin{array}{cc} 0.437 & 0.974 \\ (.016) & (.211) \\ \hline \end{array}$ |  |

Table 2 : A-efficiency and D-efficiency of some nearest neighbour balanced designs;

| ( $\mathrm{t}-5 \mathrm{r}-5$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Error <br> Model | $\begin{aligned} & \rho_{1}=.1 \\ & \rho_{2}=.1 \end{aligned}$ | $\begin{aligned} & \rho_{1}=.2 \\ & \rho_{2}=.2 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.3 \\ & \rho_{2}=.3 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.4 \\ & \rho_{2}=.4 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.5 \\ & \rho_{2}=.5 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.6 \\ & \rho_{2}=.6 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.7 \\ & \rho_{2}=.7 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.8 \\ & \rho_{2}=.8 \end{aligned}$ |  | $\begin{aligned} & \rho_{1}=.9 \\ & \rho_{2}=.9 \end{aligned}$ |  |
|  | $\alpha=0 \alpha=.5$ | $\alpha=0$ | $\alpha=.5$ | $\alpha=0$ | $\alpha=.5$ | $\alpha=0$ | $\alpha-.5$ | $\alpha=0$ | $\alpha-.5$ | $\alpha=0$ | $\alpha=.5$ | $\alpha=0$ | $\alpha=.5$ | $\alpha=0$ | $\alpha=.5$ | $\alpha=0$ | $\alpha=.5$ |
| AR(2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $E_{\text {A }}$ | $\begin{array}{cc} 1.000 & 1.000 \\ (.959) & (.982) \end{array}$ | $\begin{aligned} & 1.000 \\ & (.852) \end{aligned}$ | $\begin{aligned} & 1.000 \\ & (.936) \end{aligned}$ | $\begin{gathered} .996 \\ (.707) \end{gathered}$ | $\begin{aligned} & 1.000 \\ & (.867) \end{aligned}$ | $\begin{gathered} .989 \\ (.552) \end{gathered}$ | $\begin{aligned} & 1.000 \\ & (.781) \end{aligned}$ | $\begin{aligned} & 0.978 \\ & (.355) \end{aligned}$ | $\begin{gathered} .999 \\ (.683) \end{gathered}$ | $\begin{aligned} & 0.963 \\ & (.281) \end{aligned}$ | $\begin{gathered} .998 \\ (.571) \end{gathered}$ | $\begin{gathered} .945 \\ (.180) \end{gathered}$ | $\begin{gathered} .998 \\ (.448) \end{gathered}$ | $\begin{gathered} .924 \\ (.101) \end{gathered}$ | $\begin{gathered} .996 \\ (.312) \end{gathered}$ | $\begin{aligned} & 0.902 \\ & (.043) \end{aligned}$ | $\begin{gathered} .995 \\ (.164) \end{gathered}$ |
| $\mathrm{E}_{\mathrm{D}}$ | $\begin{array}{ll} 1.000 & 1.000 \\ (.921) & (.965) \end{array}$ | $\begin{gathered} .998 \\ (.731) \end{gathered}$ | $\begin{aligned} & 1.000 \\ & (.878) \end{aligned}$ | $\begin{gathered} .992 \\ (.513) \end{gathered}$ | $\begin{aligned} & 1.000 \\ & (.761) \end{aligned}$ | $\begin{gathered} .978 \\ (.326) \end{gathered}$ | $\begin{gathered} .999 \\ (.633) \end{gathered}$ | $\begin{gathered} .956 \\ (.155) \end{gathered}$ | $\begin{gathered} .998 \\ (.505) \end{gathered}$ | $\begin{gathered} .927 \\ (.104) \end{gathered}$ | $\begin{gathered} .997 \\ (.384) \end{gathered}$ | $\begin{gathered} .892 \\ (.052) \end{gathered}$ | $\begin{gathered} .995 \\ (.272) \end{gathered}$ | $\begin{gathered} .854 \\ (.230) \end{gathered}$ | $\begin{gathered} .993 \\ (.171) \end{gathered}$ | $\begin{gathered} .813 \\ (.008) \end{gathered}$ | $\begin{gathered} .991 \\ (.081) \end{gathered}$ |
| MA(2) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{E}_{\text {A }}$ | $\begin{array}{cc} 1.000 & 1.000 \\ (.959) & (.980) \end{array}$ | $\begin{gathered} 0.997 \\ (.828) \end{gathered}$ | $\begin{gathered} 0.997 \\ (.954) \end{gathered}$ | $\begin{gathered} 0.986 \\ (.758) \end{gathered}$ | $\begin{aligned} & 0.997 \\ & (.881) \end{aligned}$ | $\begin{gathered} 0.963 \\ (.662) \end{gathered}$ | $\begin{gathered} 0.996 \\ (.786) \end{gathered}$ | $\begin{aligned} & 0.935 \\ & (.586) \end{aligned}$ | $\begin{aligned} & 0.987 \\ & (.716) \end{aligned}$ | $\begin{aligned} & 0.899 \\ & (.531) \end{aligned}$ | $\begin{aligned} & 0.976 \\ & (.657) \end{aligned}$ | $\begin{gathered} 0.873 \\ (.494) \end{gathered}$ | $\begin{aligned} & 0.976 \\ & (.609) \end{aligned}$ | $\begin{aligned} & 0.855 \\ & (.472) \end{aligned}$ | $\begin{aligned} & 0.947 \\ & (.573) \end{aligned}$ | $\begin{aligned} & 0.844 \\ & (.460) \end{aligned}$ | $\begin{gathered} 0.933 \\ (.394) \end{gathered}$ |
| $E_{D}$ | $\begin{array}{cc} 1.000 & 1.000 \\ (.920) & (.961) \end{array}$ | $\begin{gathered} 0.994 \\ (.688) \end{gathered}$ | $\begin{aligned} & 0.995 \\ & (.911) \end{aligned}$ | $\begin{gathered} 0.973 \\ (.574) \end{gathered}$ | $\begin{aligned} & 0.994 \\ & (.774) \end{aligned}$ | $\begin{gathered} 0.993 \\ (.438) \end{gathered}$ | $\begin{aligned} & 0.992 \\ & (.617) \end{aligned}$ | $\begin{aligned} & 0.874 \\ & (.343) \end{aligned}$ | $\begin{gathered} 0.974 \\ (.513) \end{gathered}$ | $\begin{aligned} & 0.811 \\ & (.282) \end{aligned}$ | $\begin{aligned} & 0.952 \\ & (.431) \end{aligned}$ | $\begin{gathered} 0.766 \\ (.244) \end{gathered}$ | $\begin{aligned} & 0.950 \\ & (.371) \end{aligned}$ | $\begin{aligned} & 0.950 \\ & (.371) \end{aligned}$ | $\begin{aligned} & 0.898 \\ & (.328) \end{aligned}$ | $\begin{aligned} & 0.721 \\ & (.212) \end{aligned}$ | $\begin{gathered} 0.872 \\ (.138) \end{gathered}$ |

## 5. Comparison of Efficiency

In this section a quantitative measure of efficiency of the proposed designs in comparison to randomized block designs is derived. For this we assume that the covariance matrix is known except for some constant multiplier. Since the covariance matrix has to be estimated from the data, the efficiencies given here are the upper limits attainable. We compare the average variance of an elementary treatment contrast $\tau_{i}-T_{j}$ in both cases.

For a regular block design the variance of an elementary treatment contrast, estimated by ordinary least squares methods, is given by

$$
V_{1}=2 r^{-1} \sigma^{2}(1-\bar{\rho})
$$

where $\sigma^{2}$ is the variance of an observation, $\bar{\rho}$ is the average correlation between observations from any two plots within a block, the average being taken over all possible randomizations; $r$ is the number of replications.

If observations within a block follow an errors-in-variable autoregressive model, then (Williams [10])
and

$$
\sigma^{2}=\sigma_{\varepsilon}^{2}\left(1+\alpha\left(1-\rho^{2}\right)\left(1-\rho^{2}\right)^{-1}\right)
$$

$$
\bar{\rho}=\frac{2 \rho}{\left\{\left(1+\alpha\left(1-\rho^{2}\right)\right\}(t-1)(1-\rho)\right.}\left\{1-\frac{1-p^{t}}{t(1-\rho)}\right\}
$$

so that

$$
V_{1}=\frac{2 \sigma_{\varepsilon}^{2}}{r\left(1-\rho^{2}\right)}\left[1+\alpha\left(1-\rho^{2}\right)-\frac{2}{(t-1)(1-\rho)}\left\{1-\frac{\left(1-p^{t}\right)}{((1-\rho)}\right\}\right]
$$

When errors follow a first order moving average model, then

$$
V_{1}=2 r^{-1} \sigma_{\varepsilon}^{2}\left(1+\rho^{2}\right)\left(1+\frac{\alpha}{1+\rho^{2}}-\frac{2}{\left(1+\rho^{2}\right) t}\right)
$$

When errors follow first order ARMA model, then

$$
V_{1}=2 r^{-1} \sigma_{\varepsilon}^{2} r_{0}\left(1+\frac{\alpha}{r_{0}}-\frac{2}{t(t-1)} \sum_{s=1}^{(t-1)}(t-s) \gamma_{s}\right)
$$

where $\alpha=\frac{\sigma_{n}^{2}}{\sigma_{\varepsilon}^{2}}$
Table 3 : Efficiency of nearest neighbour balanced block designs in comparison to randomized block designs

| ( $\mathrm{t}-5 \mathrm{r}-5$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Error Model | $\rho=0.1$ |  | 0.2 |  | 0.3 |  | 0.4 |  | 0.5 |  | 0.6 |  | 0.7 |  | 0.8 |  | -0.9 |
| $\alpha=0 \alpha=.5 \alpha=0 \alpha-.5 \alpha=0 \alpha=.5 \alpha=0 \alpha=.5 \alpha=0 \alpha-.5 \alpha-0 \alpha-.5 \alpha=0 \alpha=.5 \alpha-0 \alpha-.5 \alpha-0 \alpha=.5$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{lllllllllllllllllllllll}\text { AR(1) } & 1.096 & 1.005 & 1.040 & 1.016 & 1.088 & 1.036 & 1.154 & 1.061 & 1.237 & 1.092 & 1.343 & 1.128 & 1.468 & 1.168 & 1.617 & 1.214 & 1.793 & 1.265\end{array}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{lllllllllllllllllllllllll}\text { MA(1) } & 1.019 & 1.010 & 1.062 & 1.030 & 1.129 & 1.059 & 1.218 & 1.114 & 1.325 & 1.132 & 1.439 & 1.186 & 1.552 & 1.229 & 1.651 & 1.269 & 1.718 & 1.302\end{array}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ARMA$(1,1)$ | $\rho_{1}=.1$ $\rho_{2}=.1$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | - 9 |
|  | $\rho_{2}=.1$ |  | - 2 |  |  |  | - 4 |  |  |  | - . 6 |  | -. 7 |  |  |  | -. 9 |
| 1.0441 .018 |  | 1.1841 .070 |  | 1.432 | 1.162 | 1.796 | 1.285 | 1.927 | 1.439 | 2.285 | 1.625 | 2.558 | 1.842 | 2.722 | 2.091 | 2.9822 .360 |  |

For generalized least squares estimation, the average variance of an elementary treatment contrast, estimated from a design $d$, is

$$
v_{2}=2(t-1)^{-1} \sum_{i=1}^{t-1} \gamma_{d i}^{-t}
$$

where $\boldsymbol{\gamma}_{\mathrm{di}}$ 's are non-zero values of $\mathrm{C}_{\mathrm{d}}$ (Kempthorne [4]).
We define the efficiency of a design d relative to a randomised block design as $\mathrm{V}_{1} / \mathrm{V}_{2}$. Table 3 shows this efficiency of complete nearest neighbour balanced block design with $t=5, r=5$.

Conclusion
The gain in efficiency of NNBD over regular block design is substantial for all the models considered when the correlation between adjacent plots ( $\rho$ ) increases. Among the models considered for the elementary treatment contrast, the NNBD under ARMA (1, 1) model shows the highest efficiency.

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